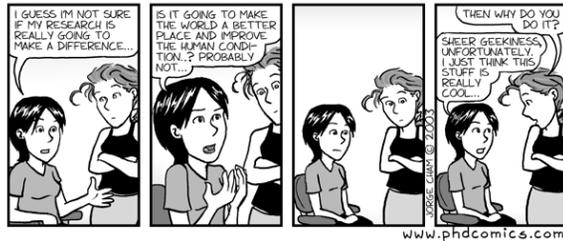


16 - everything grows! midterm summary



everything grows! - midterm summary 1

me337 - goals

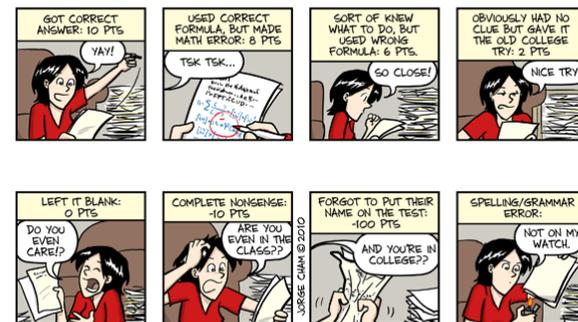
in contrast to traditional engineering structures living structures show the fascinating ability to **grow and adapt their form, shape and microstructure** to a given mechanical environment. this course addresses the phenomenon of growth on a theoretical and computational level and applies the resulting theories to classical biomechanical problems like bone remodeling, hip replacement, wound healing, atherosclerosis or in stent restenosis. this course will illustrate how classical engineering concepts like continuum mechanics, thermodynamics or finite element modeling have to be rephrased in the context of growth. having attended this course, you will be able to develop your own problemspecific finite element based numerical solution techniques and interpret the results of biomechanical simulations with the ultimate goal of improving your **understanding of the complex interplay between form and function**.

introduction 3

day	date	topic
tue	jan 07	motivation - everything grows!
thu	jan 09	basics maths - notation and tensors
tue	jan 14	project example - growing skin
thu	jan 16	kinematics - growing brains
tue	jan 21	basic kinematics - large deformation and growth
thu	jan 23	kinematics - growing hearts
tue	jan 28	kinematics - growing leaflets
thu	jan 30	basic balance equations - closed and open systems
tue	feb 04	basic constitutive equations - growing muscle
thu	feb 06	basic constitutive equations - growing tumors
tue	feb 11	volume growth - finite elements for growth - theory
thu	feb 13	volume growth - finite elements for growth - matlab
tue	feb 18	basic constitutive equations - growing bones
thu	feb 20	density growth - finite elements for growth
tue	feb 25	density growth - growing bones
thu	feb 27	everything grows! - midterm summary
tue	mar 04	midterm
thu	mar 06	remodeling - remodeling arteries and tendons
tue	mar 11	class project - discussion, presentation, evaluation
thu	mar 13	class project - discussion, presentation, evaluation
thu	mar 14	written part of final projects due

everything grows! - midterm summary 2

me 337 - grading



- 30 % homework - 3 homework assignments, 10% each
- 30 % midterm - closed book, closed notes, one single page cheat sheet
- 20 % final project oral presentations - graded by the class
- 20 % final project essay - graded by instructor

introduction 4

growth = change in mass

growth [grouθ] which is defined as **added mass**, can occur through

- hyperplasia / cell division
- hypertrophy / cell enlargement
- secretion of extracellular matrix
- accretion @external or internal surfaces

$$\text{mass} = \text{volume} \times \text{density}$$

$$\text{mass changes} = \text{volume changes} \times \text{density changes}$$

taber 'biomechanics of growth, remodeling and morphogenesis' [1995]

introduction

5

continuum mechanics

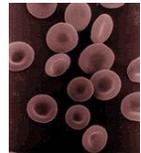
continuum hypothesis [kən'tɪn.ju.əm haɪ'pɔ:θ.ə.sɪs]
we assume that the characteristic length scale of the microstructure is much smaller than the characteristic length scale of the overall problem, such that the properties at each point can be understood as averages over a characteristic length scale

$$l^{\text{micro}} \ll l^{\text{averg}} \ll l^{\text{conti}}$$

example: biomechanics

$$l^{\text{micro}} = l^{\text{cells}} \approx 10\mu\text{m}$$

$$l^{\text{conti}} = l^{\text{tissue}} \approx 10\text{cm}$$



continuum hypothesis can be applied to analyzing tissues

introduction to continuum mechanics

6

the continuum  equations

- kinematic equations – what's strain?
general equations that characterize the deformation of a physical body without studying its physical cause
- balance equations – what's stress?
general equations that characterize the cause of motion of any body
- constitutive equations - how are they related?
material specific equations that complement the set of governing equations

$$\epsilon = \frac{\Delta l}{l}$$

$$\sigma = \frac{F}{A}$$

$$\sigma = E \epsilon$$

introduction to continuum mechanics

7

the continuum  equations

- kinematic equations - why not $\epsilon = \frac{\Delta l}{l}$?
inhomogeneous deformation » non-constant
finite deformation » non-linear
inelastic deformation » growth tensor
- balance equations - why not $\sigma = \frac{F}{A}$?
equilibrium in deformed configuration » multiple stress measures
- constitutive equations - why not $\sigma = E \epsilon$?
finite deformation » non-linear
inelastic deformation » internal variables

$$\mathbf{F} = \nabla_X \varphi$$

$$\mathbf{F} = \mathbf{F}_e \cdot \mathbf{F}_g$$

$$\text{Div}(\mathbf{P}) + \rho \mathbf{b}_0 = \mathbf{0}$$

$$\mathbf{P} = \mathbf{P}(\mathbf{F})$$

$$\mathbf{P} = \mathbf{P}(\rho, \mathbf{F}, \mathbf{F}_g)$$

introduction to continuum mechanics

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kinematic equations

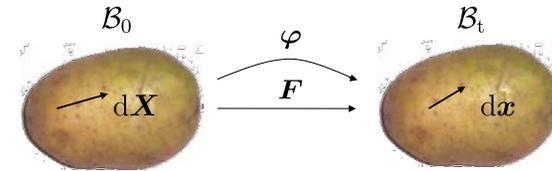
kinematic equations [kɪnə'mætɪk ɪ'kwetʃənz] describe the **motion of objects** without the consideration of the masses or forces that bring about the motion. the basis of kinematics is the choice of coordinates. the 1st and 2nd time derivatives of the position coordinates give the **velocities and accelerations**. the difference in placement between the beginning and the final state of two points in a body expresses the numerical value of **strain**. strain expresses itself as a change in size and/or shape.



kinematic equations

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kinematics equations



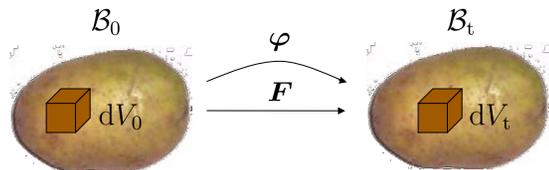
- transformation of line elements - deformation gradient F_{ij}
 $dx_i = F_{ij} dX_j$ with $F_{ij} : TB_0 \rightarrow TB_t$ $F_{ij} = \left. \frac{\partial \varphi_i}{\partial X_j} \right|_{t \text{ fixed}}$
- uniaxial tension (incompressible), simple shear, rotation

$$F_{ij}^{\text{uni}} = \begin{bmatrix} \alpha & 0 & 0 \\ 0 & \alpha^{-\frac{1}{2}} & 0 \\ 0 & 0 & \alpha^{-\frac{1}{2}} \end{bmatrix} \quad F_{ij}^{\text{shr}} = \begin{bmatrix} 1 & \gamma & 0 \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{bmatrix} \quad F_{ij}^{\text{rot}} = \begin{bmatrix} \cos(\theta) & \sin(\theta) & 0 \\ -\sin(\theta) & \cos(\theta) & 0 \\ 0 & 0 & 1 \end{bmatrix}$$

kinematic equations

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kinematic equations



- transformation of volume elements - determinant of F
 $dV_0 = d\mathbf{X}_1 \cdot [d\mathbf{X}_2 \times d\mathbf{X}_3]$ $dV_t = d\mathbf{x}_1 \cdot [d\mathbf{x}_2 \times d\mathbf{x}_3]$
 $= \det([d\mathbf{x}_1, d\mathbf{x}_2, d\mathbf{x}_3])$
 $= \det([d\mathbf{X}_1, d\mathbf{X}_2, d\mathbf{X}_3]) = \det(\mathbf{F}) \det([d\mathbf{X}_1, d\mathbf{X}_2, d\mathbf{X}_3])$
- changes in volume - determinant of deformation gradient J
 $dV_t = J dV_0$ $J = \det(\mathbf{F})$

kinematic equations

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volume growth

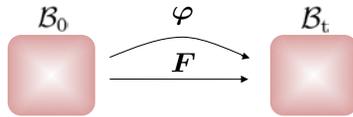
volume growth ['vɒl.ju:m grəʊθ] is conceptually comparable to thermal expansion. in linear elastic problems, growth stresses (such as thermal stresses) can be superposed on the mechanical stress field. in the nonlinear problems considered here, another approach must be used. the fundamental idea is to refer the strain measures in the constitutive equations of each material element to its current zero-stress configuration, which changes as the element grows.

taber 'biomechanics of growth, remodeling and morphogenesis' [1995]

kinematics of growth

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kinematics of finite growth

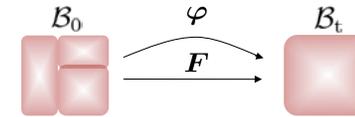


[1] consider an elastic body \mathcal{B}_0 at time t_0 , unloaded & stressfree

kinematics of growth

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kinematics of finite growth

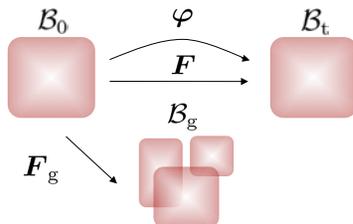


[1] consider an elastic body \mathcal{B}_0 at time t_0 , unloaded & stressfree
 [2] imagine the body is cut into infinitesimal elements each of which is allowed to undergo volumetric growth

kinematics of growth

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kinematics of finite growth

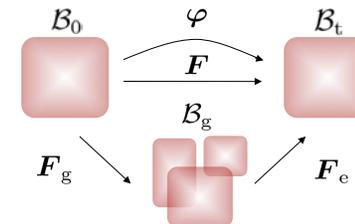


[1] consider an elastic body \mathcal{B}_0 at time t_0 , unloaded & stressfree
 [2] imagine the body is cut into infinitesimal elements each of which is allowed to undergo volumetric growth
 [3] after growing the elements, \mathcal{B}_g may be incompatible

kinematics of growth

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kinematics of finite growth

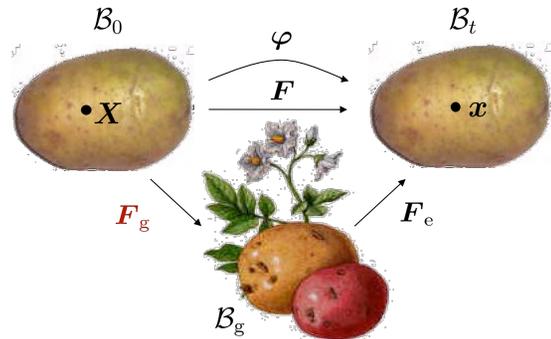


[1] consider an elastic body \mathcal{B}_0 at time t_0 , unloaded & stressfree
 [2] imagine the body is cut into infinitesimal elements each of which is allowed to undergo volumetric growth
 [3] after growing the elements, \mathcal{B}_g may be incompatible
 [4] loading generates compatible current configuration \mathcal{B}_t

kinematics of growth

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kinematics of finite growth



- incompatible growth configuration \mathcal{B}_g & growth tensor \mathbf{F}_g
 $\mathbf{F} = \mathbf{F}_e \cdot \mathbf{F}_g$

rodriguez, hoger & mc culloch [1994]

kinematics of growth

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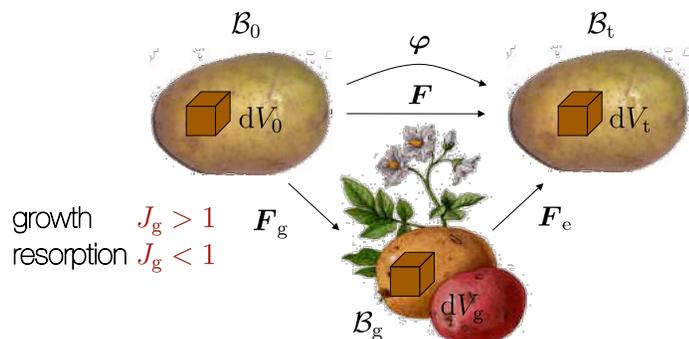
concept of incompatible growth configuration

biologically, the notion of **incompatibility** implies that subelements of the grown configuration may overlap or have gaps. the implication of incompatibility is the existence of residual stresses necessary to `squeeze` these grown subelements back together. mathematically, the notion of **incompatibility** implies that unlike the deformation gradient, $\mathbf{F} = \frac{\partial \varphi}{\partial \mathbf{X}} \Big|_{t \text{ fixed}}$ the growth tensor cannot be derived as a gradient of a vector field. incompatible configurations are useful in finite strain inelasticity such as viscoelasticity, thermoelasticity, elastoplasticity and growth.

kinematics of growth

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kinematics of finite growth



- changes in volume - determinant of growth tensor J_g
 $dV_g = J_g dV_0 \quad J_g = \det(\mathbf{F}_g)$

kinematics of growth

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kinematics – how does it grow?

- isotropic volume growth

$$\mathbf{F}^g = \vartheta \mathbf{I}$$

- transversely isotropic area growth

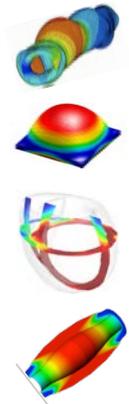
$$\mathbf{F}^g = \sqrt{\vartheta} \mathbf{I} + [1 - \sqrt{\vartheta}] \mathbf{n}_0 \otimes \mathbf{n}_0$$

- transversely isotropic fiber growth

$$\mathbf{F}^g = \mathbf{I} + [\vartheta - 1] \mathbf{f}_0 \otimes \mathbf{f}_0$$

- and various combinations thereof

$$\mathbf{F}^g = \vartheta^\perp \mathbf{I} + [\vartheta^\parallel - \vartheta^\perp] \mathbf{n}_0 \otimes \mathbf{n}_0$$



rodriguez, hoger, mc culloch [1994], taber [1995], epstein, maugin [2000], ambrosi, molica [2002], goriely, ben amar [2007], kuhl, meas, himpel, menzel [2007], socci, rennati, gervaso, vena [2007], garikipati [2009], kroon, delhaas, arts, bovenderd [2009], goktepe, abiaz, kuhl [2010], bol, albero [2014]

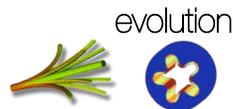
kinematics of growth

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kinetics – why does it grow?

- biochemically driven

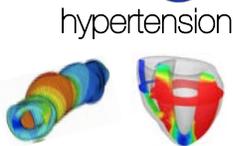
$$\dot{\vartheta}^g = k^g(\vartheta^g)$$



- stress driven

$$\dot{\vartheta}^g = k^g(\vartheta^g) \phi^g(\mathbf{M}^e)$$

$$\phi^g = \langle \text{tr}(\mathbf{M}^e) - p^{\text{crit}} \rangle$$



- strain driven

$$\dot{\vartheta}^g = k^g(\vartheta^g) \phi^g(\mathbf{F}^e)$$

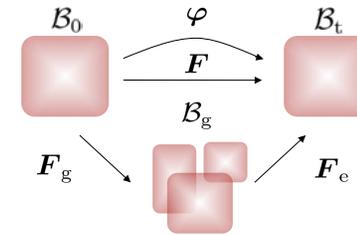
$$\phi^g = \langle \vartheta^e(\mathbf{F}^e) - \vartheta^{\text{crit}} \rangle$$



rodriguez, hoger, mc culloch [1994], taber [1995], epstein, maughn [2000], ambrosi, molica [2002], goriely, ben amar [2007], kuhl, maas, himpel, menzel [2007], socci, rennati, gervaso, vena [2007], garikipati [2009], kroon, delhaas, arts, bovendieerd[2009], goktepe, ablez, kuhl[2010], bbl, albero[2014]

kinematics of growth

kinematics of finite growth



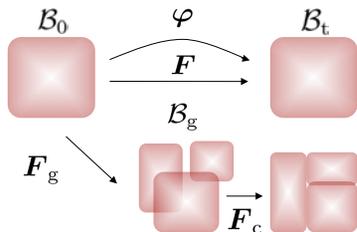
[3] after growing the elements, \mathcal{B}_g may be incompatible

[4] loading generates compatible current configuration \mathcal{B}_t

concept of residual stress

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kinematics of finite growth



[3] after growing the elements, \mathcal{B}_g may be incompatible

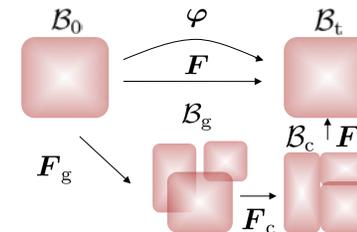
[3a] we then first apply a deformation \mathbf{F}_c to squeeze the elements back together to the compatible configuration \mathcal{B}_c

[4] to generate the compatible current configuration \mathcal{B}_t

concept of residual stress

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kinematics of finite growth



[3] after growing the elements, \mathcal{B}_g may be incompatible

[3a] we then first apply a deformation \mathbf{F}_c to squeeze the elements back together to the compatible configuration \mathcal{B}_c

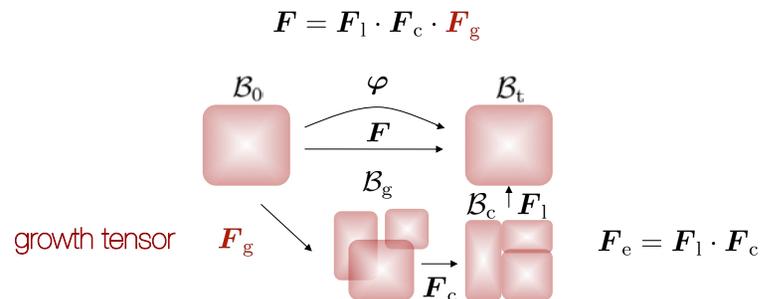
[3b] and then load the compatible configuration \mathcal{B}_c by \mathbf{F}_1

[4] to generate the compatible current configuration \mathcal{B}_t

concept of residual stress

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kinematics of finite growth



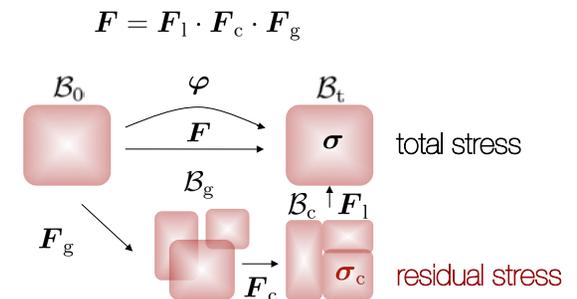
multiplicative decomposition

lee [1969], simo [1992], rodriguez, hoger & mc culloch [1994], epstein & maugin [2000], humphrey [2002], ambrosi & mollica [2002], himpel, kuhl, menzel & steinmann [2005]

concept of residual stress

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kinematics of finite growth



residual stress

the additional deformation of squeezing the grown parts back to a compatible configuration gives rise to residual stresses (see thermal stresses)

concept of residual stress

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the classical opening angle experiment



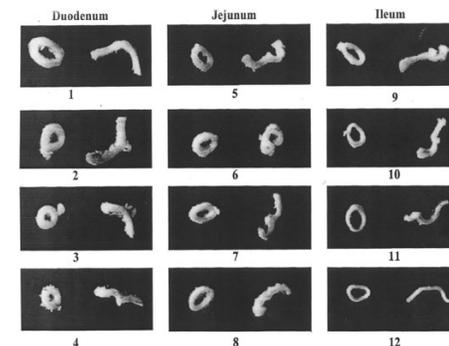
an existence of residual strains in human arteries is well known. it can be observed as an opening up of a circular arterial segment after a radial cut. an opening angle of the arterial segment is used as a measure of the residual strains generally.

fung [1990], horný, chlup, zitný, mackov [2006]

concept of residual stress

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the classical opening angle experiment



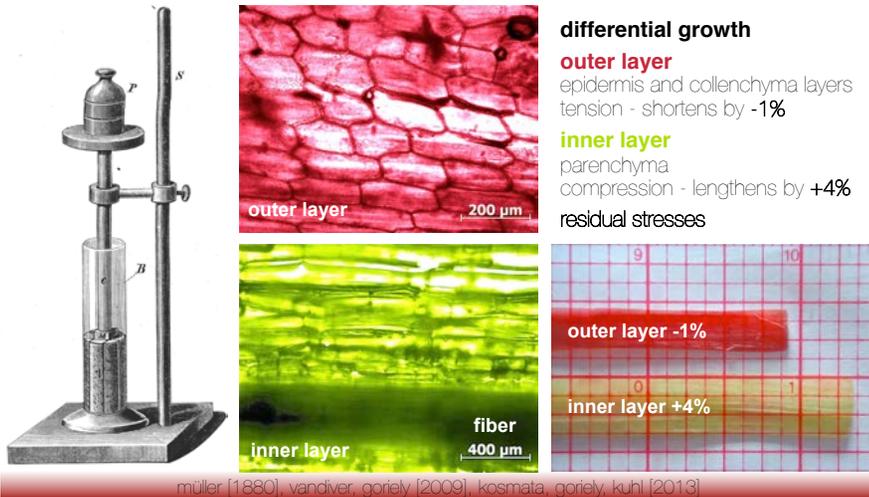
photographs showing specimens obtained from different locations in the intestine in the no-load state (left, closed rings) and the zero-stress state (right, open sectors). the rings of jejunum (site 5 to site 8) turned inside out when cut open

zhao, sha, zhuang, gregersen [2002]

concept of residual stress

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residual stress in rhubarb



müller [1880], vandiver, goriely [2009], kosmala, goriely, kuhl [2013]

concept of residual stress

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constrained growth during development

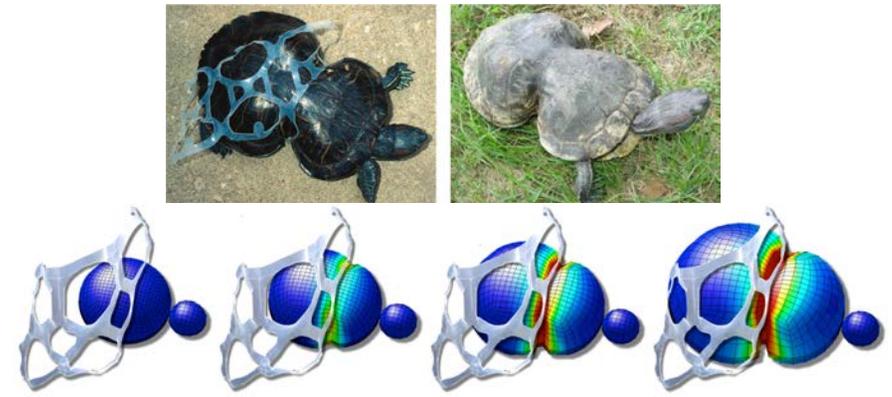


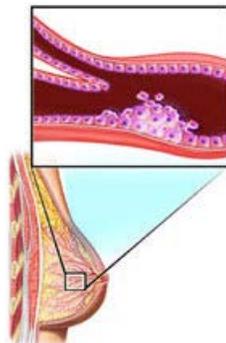
figure. growth-induced microenvironmental changes in a nine-year old female red-eared slider turtle trapped in a plastic six-pack ring. the turtle had worn the ring for five years. during this time, the ring had constrained the growth of the outer shell and created growth-induced stresses on the inner organs.

example - growing turtles



volume growth - cylindrical tumor

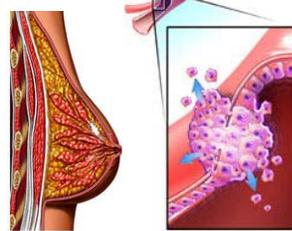
normal cells grow and multiply at a specific rate. cells that grow and multiply without stopping are called cancerous or malignant. however, they are not detectable when they first start growing.



invasive or infiltrating ductal carcinoma is the most common type of breast cancer. it occurs when the cells that line the milk duct become abnormal and spread into the surrounding breast tissue.

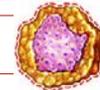


ductal carcinoma in situ is a non-invasive change in the cells that line the milk tubes that bring milk from the milk lobules to the nipple



example - breast cancer

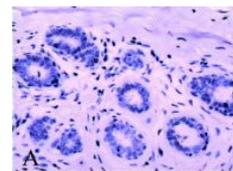
31



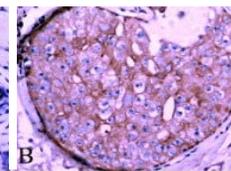
volume growth - cylindrical tumor

model assumptions

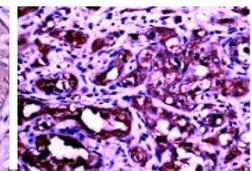
- ductal carcinoma - tumor grows in breast duct for up to 10 cm
- model - homogeneous growth inside a rigid cylinder
- assumption - rotational symmetry
- strategy - solve for deformation that satisfies equilibrium and boundary conditions



normal ductal epithelial cells (negative)



tumor cells of ductal carcinoma (positive)



invasive ductal carcinoma cells (strongly positive)

kinematic coupling of growth and deformation

example - breast cancer

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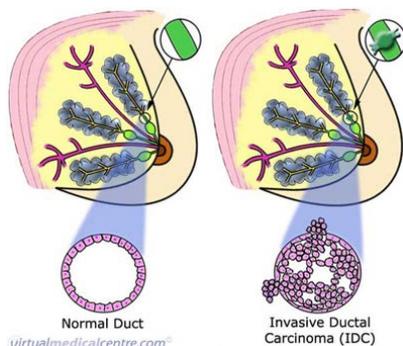
volume growth - cylindrical tumor

- homogeneous deformation inside a rigid cylinder

$$x = X \quad y = Y \quad z = \lambda Z$$

- deformation gradient

$$\mathbf{F} = \nabla_X \varphi \quad \mathbf{F} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & \lambda \end{bmatrix}$$



Normal Duct

Invasive Ductal Carcinoma (IDC)

virtualmedicalcentre.com

kinematic coupling of growth and deformation

example - breast cancer

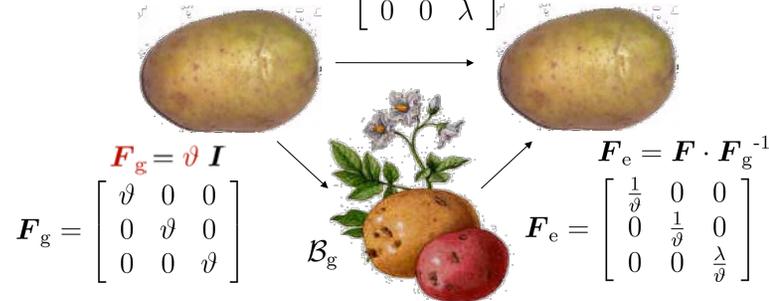
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volume growth - cylindrical tumor

$$\mathbf{F} = \nabla_X \varphi$$

$$\mathbf{F} = \begin{bmatrix} 1 & 0 & 0 \\ 0 & 1 & 0 \\ 0 & 0 & \lambda \end{bmatrix}$$



$$\mathbf{F}_{\sigma_g} = \begin{bmatrix} \vartheta & 0 & 0 \\ 0 & \vartheta & 0 \\ 0 & 0 & \vartheta \end{bmatrix}$$

$$\mathbf{F}_e = \begin{bmatrix} \frac{1}{\vartheta} & 0 & 0 \\ 0 & \frac{1}{\vartheta} & 0 \\ 0 & 0 & \frac{\lambda}{\vartheta} \end{bmatrix}$$

ambrosi & molica [2002]

example - breast cancer

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volume growth - cylindrical tumor

- stress

$$\boldsymbol{\sigma}_e = \begin{bmatrix} \sigma_{xx} & 0 & 0 \\ 0 & \sigma_{yy} & 0 \\ 0 & 0 & \sigma_{zz} \end{bmatrix}$$

$$\sigma_{xx} = \sigma_{yy} = \mu \frac{\vartheta^3}{\lambda} \left[\frac{1}{\vartheta^2} - \left[\frac{\lambda}{\vartheta^3} \right]^q \right]$$

$$\sigma_{zz} = \mu \frac{\vartheta^3}{\lambda} \left[\frac{\lambda^2}{\vartheta^2} - \left[\frac{\lambda}{\vartheta^3} \right]^q \right]$$

$$\sigma_{zz} = 0$$

- bc's

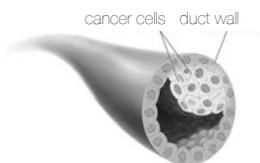
- axial displacement λ as a function of growth ϑ

$$\lambda = \vartheta^{[2-3q]/[2-q]}$$

- growth induced stress σ_{xx} on tumor wall

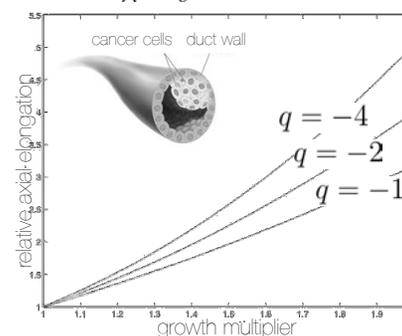
$$\sigma_{xx} = \mu \left[\vartheta^{2q/[2-q]} - \vartheta^{[4-4q]/[2-q]} \right]$$

ambrosi & molica [2002]

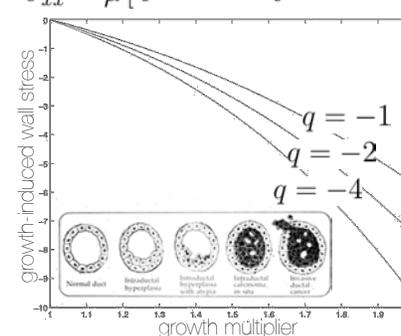


volume growth - cylindrical tumor

$$\lambda = \vartheta^{[2-3q]/[2-q]}$$



$$\sigma_{xx} = \mu \left[\vartheta^{2q/[2-q]} - \vartheta^{[4-4q]/[2-q]} \right]$$



tumor pressure on duct walls increases with growth

ambrosi & molica [2002]

example - breast cancer

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example - breast cancer

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balance equations

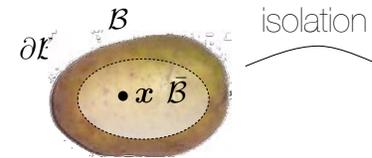
balance equations [ˈbæl.əns ɪˈkweɪ.ʒəns] of mass, momentum, angular momentum and energy, supplemented with an entropy inequality constitute the set of conservation laws. the law of **conservation of mass/matter** states that the **mass of a closed system** of substances will remain **constant**, regardless of the processes acting inside the system. the principle of conservation of momentum states that the total momentum of a closed system of objects is constant.



balance equations

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balance equations

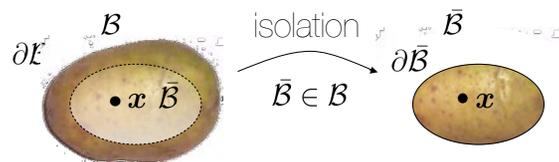


[1] isolation of subset \bar{B} from B

balance equations

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balance equations



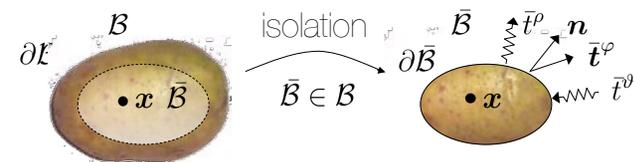
[1] isolation of subset \bar{B} from B

[2] characterization of influence of remaining body through phenomenological quantities - contact fluxes \bar{t}^ρ , \bar{t}^φ & \bar{t}^θ

balance equations

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balance equations



[1] isolation of subset \bar{B} from B

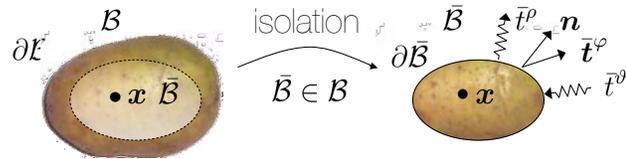
[2] characterization of influence of remaining body through phenomenological quantities - contact fluxes \bar{t}^ρ , \bar{t}^φ & \bar{t}^θ

[3] definition of basic physical quantities - mass, linear and angular momentum, energy

balance equations

40

balance equations

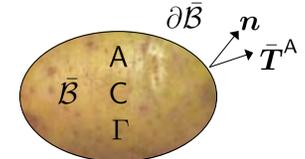


- [1] isolation of subset $\bar{\mathcal{B}}$ from \mathcal{B}
- [2] characterization of influence of remaining body through phenomenological quantities - contact fluxes $\bar{\mathbf{t}}^\rho$, $\bar{\mathbf{t}}^\varphi$ & $\bar{\mathbf{t}}^\theta$
- [3] definition of basic physical quantities - mass, linear and angular momentum, energy
- [4] postulation of balance of these quantities

balance equations

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generic balance equation - closed systems



general format

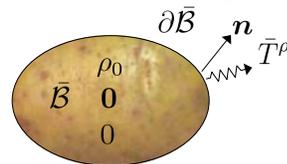
- A ... balance quantity
- B ... flux $\mathbf{B} \cdot \mathbf{n} = \bar{\mathbf{T}}^A$
- C ... source
- Γ ... production

$$D_t A = \text{Div}(\mathbf{B}) + C + \Gamma$$

balance equations

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balance of mass - closed systems



balance of mass

ρ_0 ... density

$\mathbf{0}$... no mass flux

0 ... no mass source

0 ... no mass production

$$\bar{\mathbf{T}}^\rho = \mathbf{0}$$

continuity equation $D_t \rho_0 = 0$

balance equations

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thermodynamic systems - open systems

open system ['ou.pən 'sɪs.təm] thermodynamic system which is allowed to exchange mechanical work, heat and mass, typically $\mathbf{P} = \mathbf{P}(\nabla\varphi, \dots)$, $\mathbf{Q} = \mathbf{Q}(\nabla\theta, \dots)$ and $\mathbf{R} = \mathbf{R}(\nabla\rho, \dots)$ with its environment. enclosed by a deformable, diathermal, permeable membrane. characterized through its state of deformation φ , temperature θ and density ρ .

balance equations

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balance of mass - open systems

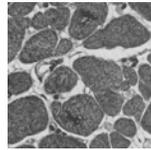
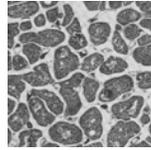
$$D_t \rho_0 = \text{Div}(\mathbf{R}) + \mathcal{R}_0$$

mass flux \mathbf{R}

- cell movement (migration)

mass source \mathcal{R}_0

- cell growth (proliferation)
- cell division (hyperplasia)
- cell enlargement (hypertrophy)



biological equilibrium

cowin & hegedus [1976], beaupré, orr & carter [1990], harrigan & hamilton [1992], jacobson, levenston, beaupré, simo & carter [1995], huiskes [2000], carter & beaupré [2001]

balance equations

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constitutive equations

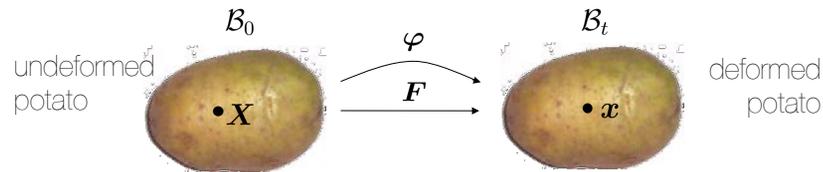
constitutive equations [kən'stɪ.tu.tɪv ɪ'kwet.ʃəns] in structural analysis, constitutive relations **connect applied stresses** or forces to **strains** or deformations. the constitutive relations for linear materials are linear. more generally, in physics, a constitutive equation is a relation between two physical quantities (often tensors) that is specific to a material, and does not follow directly from physical law. some constitutive equations are **simply phenomenological**; others are **derived from first principles**.



constitutive equations

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neo hooke'ian elasticity

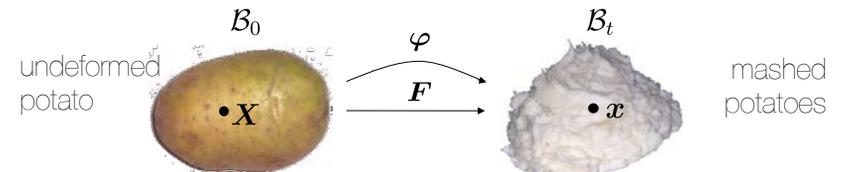


- free energy $\psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 \ln^2(\det(\mathbf{F})) + \frac{1}{2} \mu_0 [\mathbf{F}^t \cdot \mathbf{F} : \mathbf{I} - n^{\text{dim}} - 2 \ln(\det(\mathbf{F}))]$
- definition of stress $\mathbf{P}^{\text{neo}} = D_{\mathbf{F}} \psi_0^{\text{neo}} = \mu_0 \mathbf{F} + [\lambda_0 \ln(\det(\mathbf{F})) - \mu_0] \mathbf{F}^{-t}$

constitutive equations

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neo hooke'ian elasticity



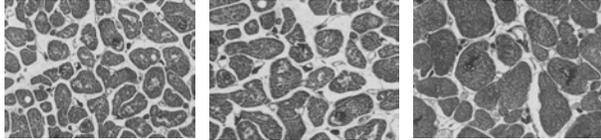
- free energy ~~$\psi^{\text{neo}} = \frac{1}{2} \lambda \ln^2(\det(\mathbf{F})) + \frac{1}{2} \mu [\mathbf{F}^t \cdot \mathbf{F} : \mathbf{I} - n^{\text{dim}} - 2 \ln(\det(\mathbf{F}))]$~~
- definition of stress ~~$\mathbf{P}^{\text{neo}} = \rho_0 D_{\mathbf{F}} \psi = \mu \mathbf{F} + [\lambda \ln(\det(\mathbf{F})) - \mu] \mathbf{F}^{-t}$~~
- remember! mashing potatoes is not an elastic process!

constitutive equations

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volume growth at constant density

- free energy $\psi_0 = \psi_0^{\text{neo}}(\mathbf{F}_e)$
- stress $\mathbf{P}_e = \mathbf{P}_e^{\text{neo}}(\mathbf{F}_e)$
- growth tensor $\mathbf{F}_g = \vartheta \mathbf{I}$ $D_t \vartheta = k_\vartheta(\vartheta) \text{tr}(\mathbf{C}_e \cdot \mathbf{S}_e)$
growth function pressure
- mass source $\mathcal{R}_0 = 3 \rho_0 \vartheta^2 D_t \vartheta$
increase in mass



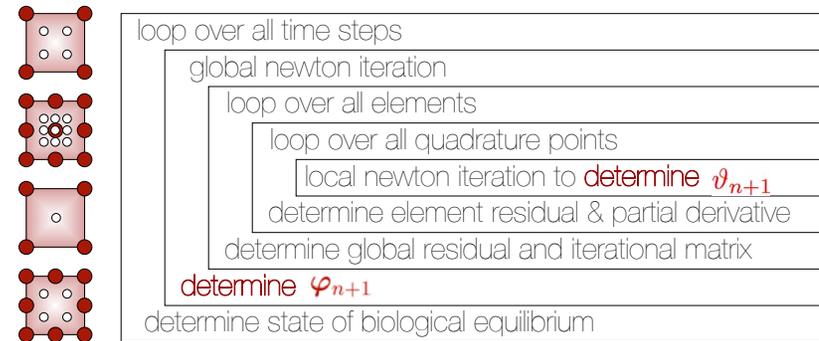
kinematic coupling of growth and deformation

rodriguez, hoger & mc culloch [1994], epstein & maugin [2000], humphrey [2002]

volume growth

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integration point based solution of growth equation



growth multiplier ϑ as internal variable

volume growth - finite element method

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in-stent restenosis

restenosis is the reoccurrence of stenosis, the narrowing of a blood vessel, leading to restricted blood flow. restenosis usually pertains to a blood vessel that has become narrowed, received treatment, and subsequently became renarrowed. in some cases, surgical procedures to widen blood vessels can cause further narrowing. during balloon angioplasty, the balloon 'smashes' the plaques against the arterial wall to widen the size of the lumen. however, this damages the wall which responds by using physiological mechanisms to repair the damage and the wall thickens.

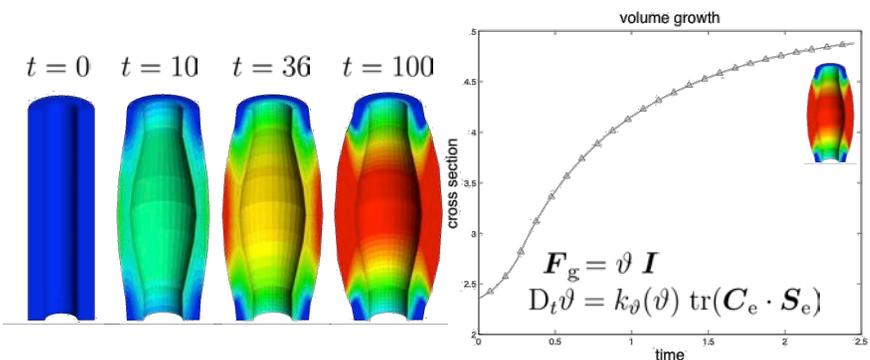


example - stenting and restenosis

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qualitative simulation of stent implantation



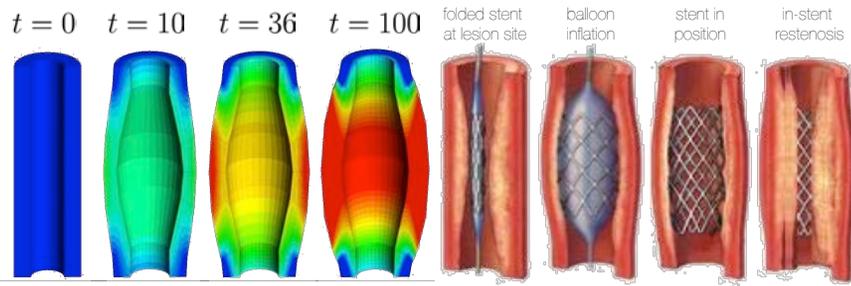
stress-induced volume growth

kuhl, maas, himpel & menzel [2007]

example - stenting and restenosis

52

qualitative simulation of stent implantation



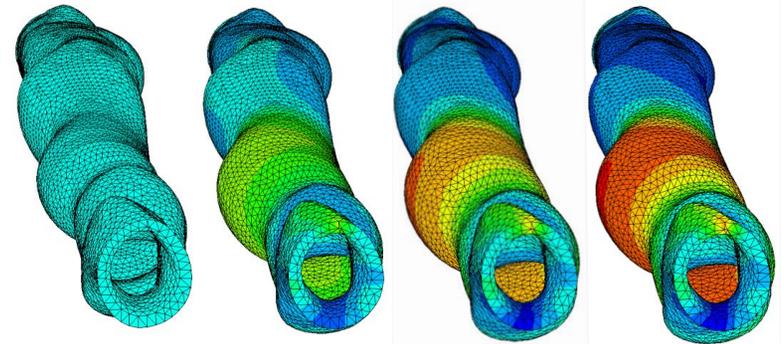
stress-induced volume growth

kuhl, maas, himpel & menzel [2007]

example - stenting and restenosis

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virtual stent implantation - patient specific model



tissue growth - response to virtual stent implantation

kuhl, maas, himpel & menzel [2007]

example - stenting and restenosis

54



skin expansion

skin expansion is a technique used by plastic and restorative surgeons to cause the body grow additional skin. Keeping living tissues under tension causes new cells to form and the amount of tissue to increase. In some cases, this may be accomplished by the implantation of inflatable balloons under the skin. By far the most common method, the surgeon inserts the inflatable expander beneath the skin and periodically, over weeks or months, injects a saline solution to slowly stretch the overlying skin. The growth of tissue is permanent, but will retract to some degree when the expander is removed. Within the past 30 years, skin expansion has revolutionized reconstructive surgery. Typical applications are breast reconstruction, burn injuries, and pediatric plastic surgery.



example - skin expansion

55

skin expansion and growth - facial reconstruction



In this study of reconstruction of the forehead in children, the average number of surgical procedures required to complete reconstruction was six, involving an average of three tissue expansion procedures.

gosain & cortes [2007]

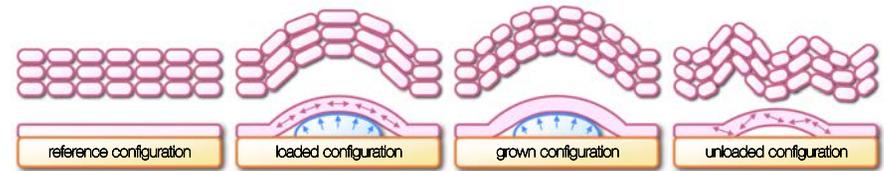
example - skin expansion

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example - skin expansion

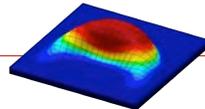
schematic sequence of tissue expansion



at biological equilibrium, the skin is in a physiological state of resting tension. a tissue expander is implanted subcutaneously between the skin and the hypodermis. when the expander is inflated, mechanical stretch induces cell proliferation causing the skin to grow. growth restores the state of resting tension. expander deflation reveals residual stresses in the skin layer.

example - skin expansion

volume growth at constant density



- deformation gradient

$$\mathbf{F} = \mathbf{F}^e \cdot \mathbf{F}^g \quad \text{with} \quad \mathbf{F} = \nabla_{\mathbf{x}} \varphi$$

- jacobians ... remember: volume change

$$J = J^e J^g \quad \text{with} \quad J = \det(\mathbf{F})$$

$$J^e = \det(\mathbf{F}^e) \quad \text{and} \quad J^g = \det(\mathbf{F}^g)$$

- area change

$$\vartheta = \vartheta^e \vartheta^g \quad \text{with} \quad \vartheta = \|\text{cof}(\mathbf{F}) \cdot \mathbf{n}_0\|$$

$$\vartheta^e = \|\text{cof}(\mathbf{F}^e) \cdot \mathbf{n}_0\| \quad \text{and} \quad \vartheta^g = \|\text{cof}(\mathbf{F}^g) \cdot \mathbf{n}_0\|$$

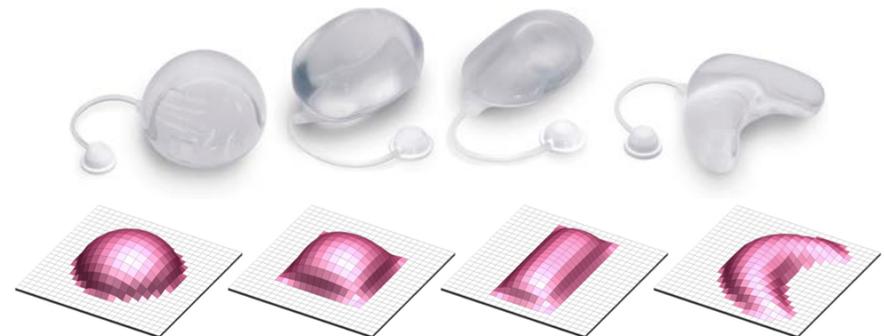
- growth tensor ... growth = area change

$$\mathbf{F}^g = \sqrt{\vartheta^g} \mathbf{I} + [1 - \sqrt{\vartheta^g}] \mathbf{n}_0 \otimes \mathbf{n}_0$$

the adrian model [2010]

example - skin expansion

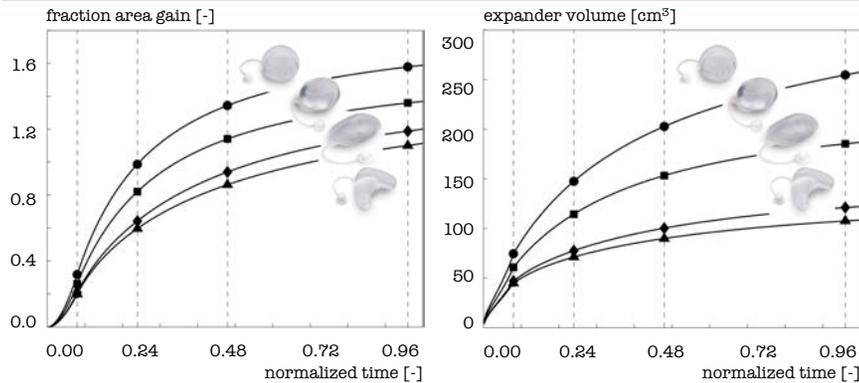
skin expander inflation and deflation



skin is modeled as a 0.2cm thin 12x12cm² square sheet, discretized with 3x24x24=1728 trilinear brick elements, with 4x25x25=2500 nodes and 7500 degrees of freedom. the base surface area of all expanders is scaled to 148 elements corresponding to 37cm². this area, shown in red, is gradually pressurized from below while the bottom nodes of all remaining elements, shown in white, are fixed.

example - skin expansion

area gain and expander volume

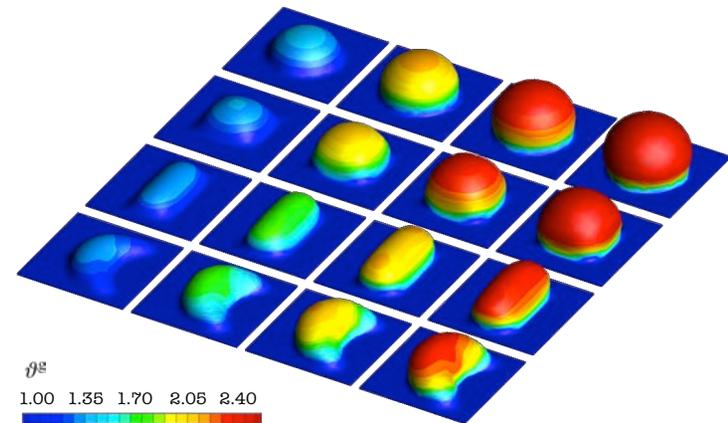


tissue expander inflation. expanders are inflated gradually between $t=0.00$ and $t=0.08$ by linearly increasing the pressure, which is then held constant from $t=0.08$ to $t=1.00$ to allow the skin to grow. under the same pressure, the circular expander displays the largest fractional area gain and expander volume, followed by the square, the rectangular, and the crescent-shaped expanders.

example - skin expansion

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area growth – comparison of four expanders

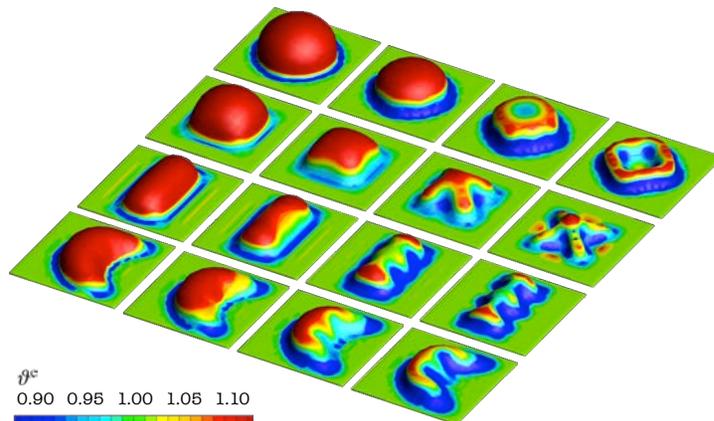


tissue expander inflation. spatio-temporal evolution of area growth. under the same pressure applied to the same base surface area, the circular expander induces the largest amount of growth followed by the square, the rectangular, and the crescent-shaped expanders.

example - skin expansion

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elastic area stretch – comparison of four expanders



tissue expander deflation. spatio-temporal evolution of elastic area stretch. as the expander pressure is gradually removed, from left to right, the grown skin layer collapses. deviations from a flat surface after total unloading, right, demonstrate the irreversibility of the growth process.

example - skin expansion

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stretch-induced muscle fiber lengthening

- deformation gradient

$$\mathbf{F} = \mathbf{F}^e \cdot \mathbf{F}^g \quad \text{with} \quad \mathbf{F} = \nabla_X \boldsymbol{\varphi}$$



- volume change

$$J = J^e J^g \quad \text{with} \quad J = \det(\mathbf{F}) > 0$$

- fiber stretch

$$\lambda = \lambda^e \lambda^g \quad \text{with} \quad \lambda = [\mathbf{n}_0 \cdot \mathbf{F}^t \cdot \mathbf{F} \cdot \mathbf{n}_0]^{1/2}$$

- growth tensor

$$\mathbf{F}^g = \mathbf{I} + [\vartheta - 1] \mathbf{n}_0 \otimes \mathbf{n}_0 \quad \vartheta = \lambda^g$$

zöllner, ablez, böhl, kuhl [2012]

example – muscle lengthening

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stretch-induced muscle fiber lengthening

- growth tensor

$$\mathbf{F}^g = \mathbf{I} + [\vartheta - 1] \mathbf{n}_0 \otimes \mathbf{n}_0$$

- fiber lengthening

$$\dot{\vartheta} = k(\vartheta) \phi(\lambda^e)$$

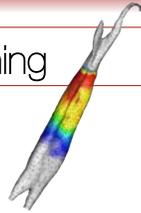
- weighting function

$$k^g = [[\vartheta^{\max} - \vartheta^g]/[\vartheta^{\max} - 1]]^\gamma / \tau$$

- growth criterion

$$\phi = \langle \lambda^e - \lambda^{\text{crit}} \rangle = \langle \lambda / \vartheta - \lambda^{\text{crit}} \rangle$$

zöllner, abiez, böhl, kuhl [2012]



example – muscle lengthening

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example 01 - limb lengthening

limb lengthening is a highly invasive surgical procedure to reconstruct or correct congenital and developmental deformities, post-traumatic injuries, regions of tumor removal, and **short stature**. using the principle of **distraction osteogenesis**, the surgeon cuts the bone in two and gradually pulls apart the two ends, triggering new bone to form. while the **main goal of osteodistraction is to lengthen the bone** itself, it is key to the procedure that the **surrounding muscle grows in parallel** with the stretched bone. contracture, the lack of appropriate muscle adaptation, is a



major source of complication during limb lengthening. optimal results can be obtained by lengthening the bone at a rate of **1mm per day, up to no more than 20%** of its initial length. although it is well accepted that mechanical factors play a limiting role in bone lengthening, to date, there are no mechanistic models that provide a scientific interpretation of these **empirical guidelines**.

example – muscle lengthening

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limb lengthening experiment in rabbits

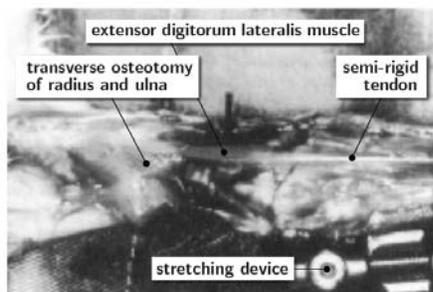


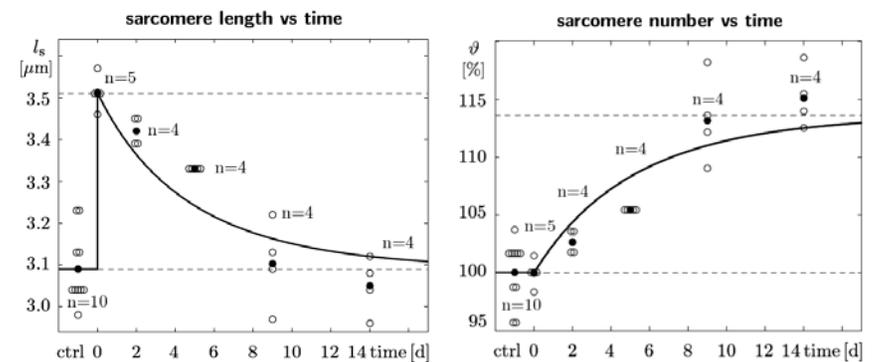
Figure 2. Stretching skeletal muscle. In a controlled limb lengthening model in rabbits, the radius and the ulna of the left forearm are lengthened by 4% inducing a stretch of $\lambda = 1.14$ in the extensor digitorum lateralis muscle. Chronic eccentric muscle growth through sarcomerogenesis is characterized in situ using light diffraction imaging. Adopted with permission from [33].

matano, tamai, kurokawa [1994], zöllner, abiez, böhl, kuhl [2012]

example - stretching skeletal muscle

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stretching of extensor digitorum lateralis muscle

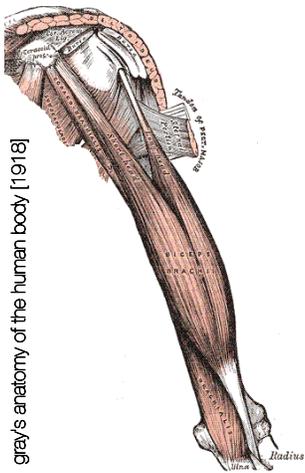


zöllner, abiez, böhl, kuhl [2012]

example – stretching skeletal muscle

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example 02 – tendon tear



in contrast to limb lengthening, **tendon lengthening**, **tendon transfer**, and **tendon reattachment** after **tendon tear** are surgical procedures, which directly manipulate the muscle-tendon complex to correct posture or gait, and to improve or restore force generation. typically, these corrections are performed in a **single-step procedure**, which permits the muscle to regain its original architecture. recent studies suggest that a restoration of normal architecture and physiological function might be possible through a **gradual lengthening** of the musculotendinous unit when stretched at a rate of **1mm per day**. while we can sufficiently well approximate the short-term response to these surgical procedures by kinematic models, we are currently unable to predict their long-term behavior through chronic muscle adaptation.

example - stretching skeletal muscle

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stretching of biceps brachii muscle

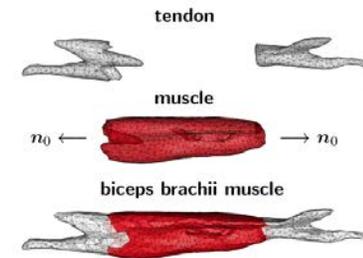


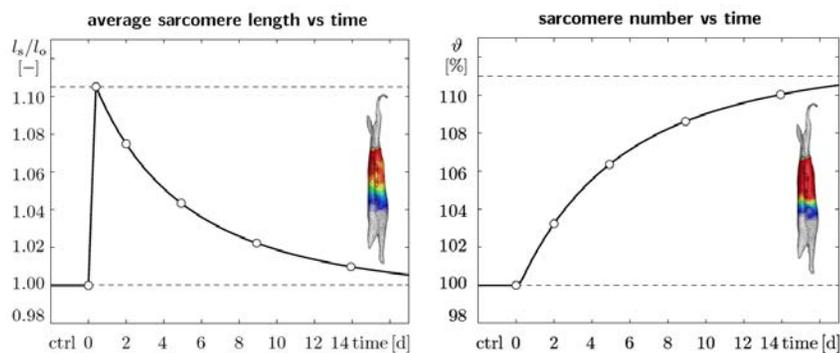
Figure 7. Biceps brachii muscle. The finite element model reconstructed from magnetic resonance images consists of 2,705 nodes and a total of 11,816 linear tetrahedral elements. The muscle, discretized by 9,393 elements (red), is attached to the elbow (left) and to the shoulder (right) through the distal and proximal biceps tendons, discretized by 2,423 elements (gray). The biceps brachii is a classical fusiform muscle with fibers n_0 arranged in parallel bundles along its long axis [6].

zöllner, abelez, böhl, kuhl [2012]

example – stretching skeletal muscle

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serial sarcomere length vs time

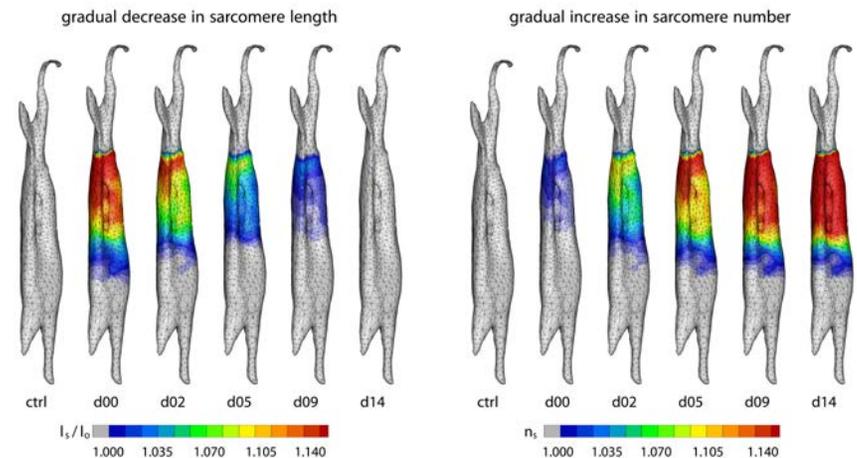


zöllner, abelez, böhl, kuhl [2012]

example – stretching skeletal muscle

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serial sarcomere length vs time



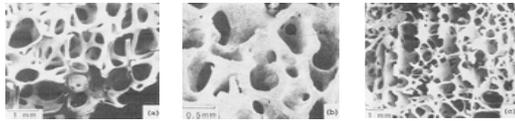
zöllner, abelez, böhl, kuhl [2012]

example – stretching skeletal muscle

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density growth at constant volume

- free energy $\psi_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^n \psi_0^{\text{neo}}(\mathbf{F})$
- stress $\mathbf{P} = \left[\frac{\rho_0}{\rho_0^*} \right]^n \mathbf{P}^{\text{neo}}(\mathbf{F})$
- mass flux $\mathbf{R} = R_0 \nabla_X \rho_0$
- mass source $\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0(\mathbf{F}) - \psi_0^*$



constitutive coupling of growth and deformation

gibson & ashby [1999]

density growth

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staggered solution - integration point based



weinans, huiskes & grootenboer [1992], harrigan & hamilton [1992], [1994], jacobs, levenston, beaupré, simo & carter [1995]

simultaneous solution - node point based



jacobs, levenston, beaupré, simo & carter [1995], fischer, jacobs, levenston & carter [1997], nackenhorst [1997], levenston [1997]

sequential solution - element based

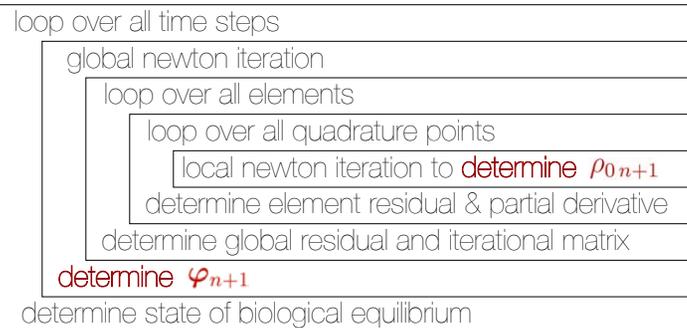
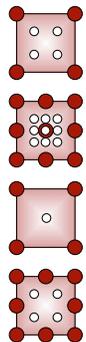


huiskes, weinans, grootenboer, dalstra, fudala & slooff [1987], carter, orr, fhyrie [1989], beaupré, orr & carter [1990], weinans, huiskes & grootenboer [1992], [1994], jacobs, levenston, beaupré, simo & carter [1995], huiskes [2000], carter & beaupré [2001]

density growth - finite element method

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integration point based solution of growth equation

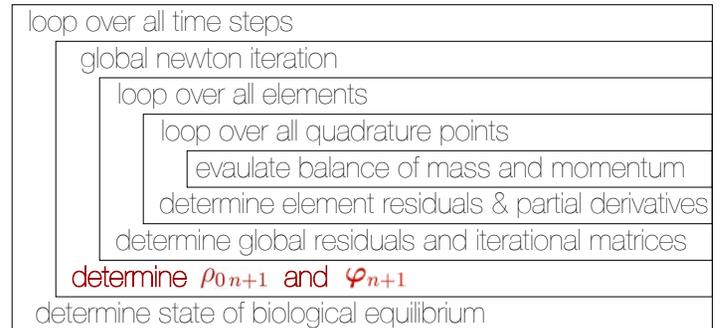
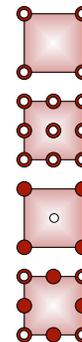


density ρ_0 as internal variable

density growth - finite element method

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node point based solution of growth equation

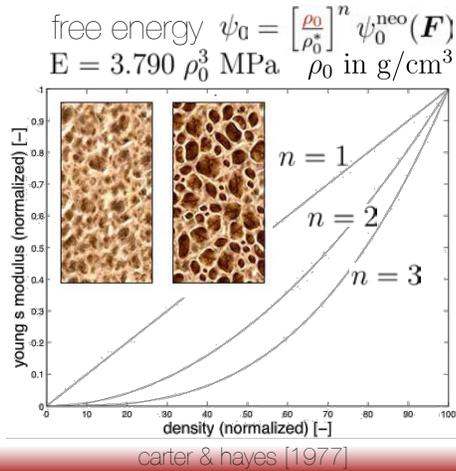


density ρ_0 as nodal degree of freedom

density growth - finite element method

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neo hooke'ian elasticity of bone as a cellular material



example – bone loss in space

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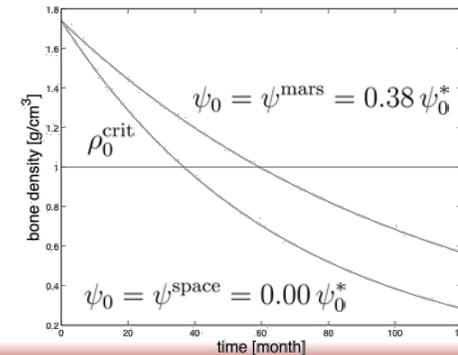


density growth - bone loss in space



$$D_t \rho_0 = c \rho_0 \left[\frac{\psi_0}{\psi_0^*} - 1 \right] \quad D_t \rho_0 = \frac{1}{\Delta t} [\rho_0^{n+1} - \rho_0^n]$$

$$\rho_0^{n+1} = \rho_0^n + c \rho_0^n \left[\frac{\psi_0}{\psi_0^*} - 1 \right] \Delta t \quad \rho_0(t_0) = 1.79 \frac{\text{g}}{\text{cm}^3}$$



$$\rho_0(36) = 1.0098$$

$$\rho_0(37) = 0.9947$$



example - bone loss in space

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tennis player's arm

Purpose

It is well known that exercise-induced loads cause bone hypertrophy in the dominant arm of tennis players; this phenomenon has been documented by numerous studies of players who began play at pre-pubescent ages¹⁻³. However, the details that describe the processes of growth and remodeling that accompany this observation are unknown⁴⁻⁷.

In addition, it is unclear as to which are the dominant variables that shape bone growth: muscular loading, impact forces during play or biological factors. We hypothesize that we can model this bone hypertrophy using a finite element growth model and that simulation gives further insight into the interplay between load and biological response.

Methods

Figure 2: Observation of serve posture suggests that humerus remains aligned with shoulders throughout serve. Humerus rotation is identified as most critical motion influencing bone growth in tennis players.

Figure 3: Critical serve posture at moment of racket-ball contact.

Figure 4: Meshed humerus in OpenSim (left) and finite element mesh (right) with 1192 nodes and 4362 linear tetrahedral elements.

Figure 5: Density changes with increasing number of load cycles.

Results

A three dimensional finite element model of the human humerus has been generated. Three dimensional muscle force vectors, muscle attachment points and boundary conditions for the finite element simulation have been determined based on video analysis with the help of OpenSim. The finite element simulation based on strain energy driven bone growth reveals pronounced localized increase in bone density in the dominant right arm. The results of the simulation of Figure 6 are in qualitatively good agreement with the bone mass density scans displaced in Figure 1.

Figure 6: Variation in humerus density in left and right arm of professional tennis player. Finite element simulation.

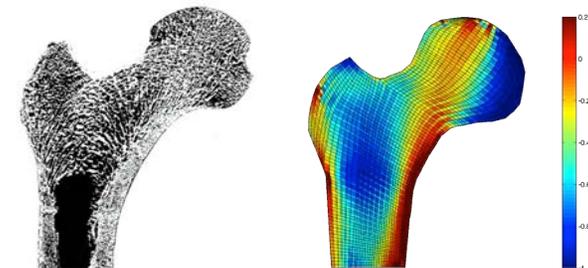
Conclusions

The encouraging results of our study could be of equal benefit to high performance athletes and patients with degenerative bone diseases. Based on patient-specific studies, optimized training strategies can be developed to promote bone growth.

example - tennis player's arm

functional adaptation of proxima femur

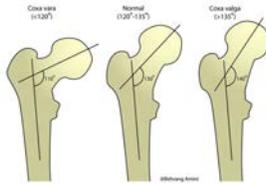
$$D_t \rho_0 = \mathcal{R}_0 \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m} \psi_0 - \psi_0^*$$



the density develops such that the tissue can just support the given mechanical load

example - growing bone

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femoral neck deformity

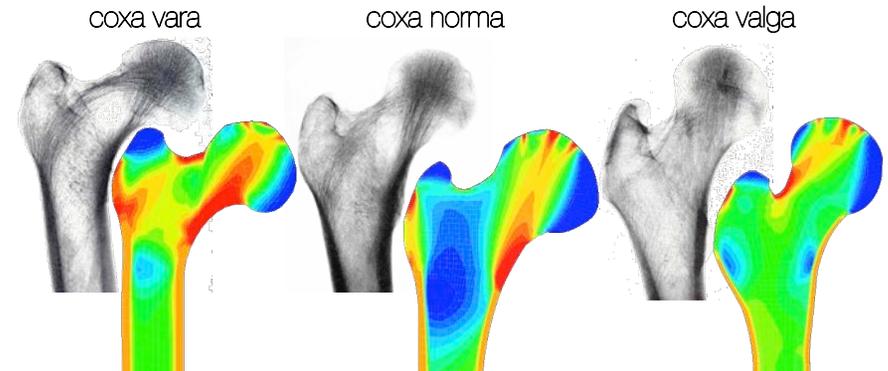
the femoral neck normally forms an angle of 120-135 degrees with the shaft of the bone. this acts as the lever in easing the action of the muscles around the hip joint. an increase or decrease in this angle beyond the normal limits causes improper action of muscles, and interferes with walking. an increase in the angle beyond 135 degrees is called **coxa valga** or outward curvature of the hip joint. a decrease in the angle below 120 degrees is called **coxa vara** or inward curvature of the hip joint.



example - femoral neck deformity

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simulation vs. x-ray scans



excellent agreement of simulation and x-ray pattern

pauwels [1973], balle [2004], kuhl & balle [2005]

example - femoral neck deformity

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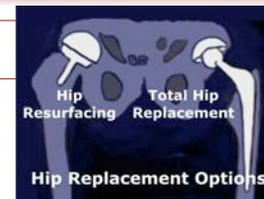
total hip replacement vs hip resurfacing



- about 120,000 artificial hip replacements in us per year
- **aseptic loosening** caused by **adaptive bone remodeling**
- goal prediction of **dredistribution of bone density**

example - hip replacement

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total hip replacement

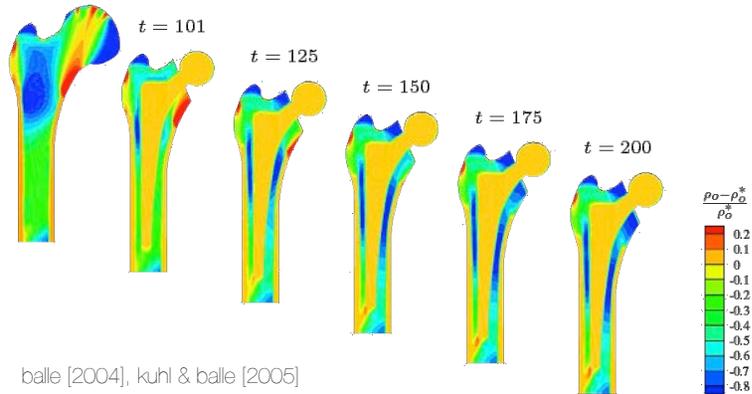
total hip replacement is a surgical procedure in which the hip joint is replaced by a prosthetic implant. a total hip replacement consists of replacing both the acetabulum and the femoral head. hip replacement is currently the most successful and reliable orthopaedic operation. risks and complications include aseptic loosening, dislocation, and pain. in the long term, many problems relate to **bone resorption and subsequent loosening** or fracture often requiring revision surgery.



example - hip replacement

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conventional total hip replacement



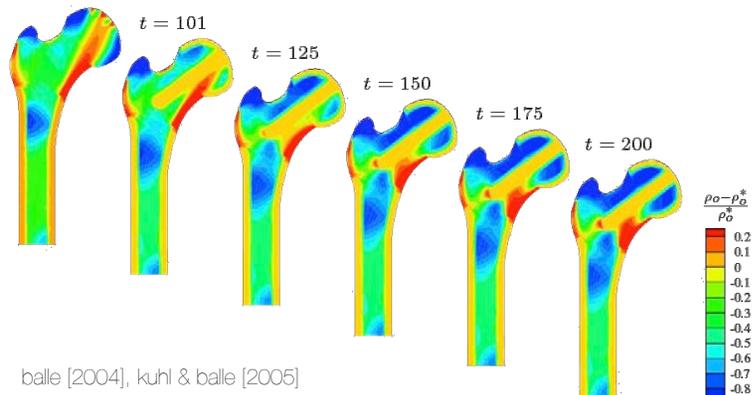
balle [2004], kuhl & balle [2005]

stress shielding • bone resorption • implant loosening

example - hip replacement

85

new birmingham hip resurfacing

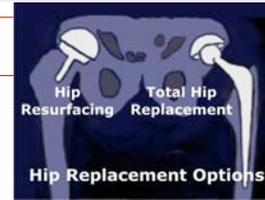


balle [2004], kuhl & balle [2005]

improved ingrowth • anatomic situation • less resorption

example - hip replacement

87



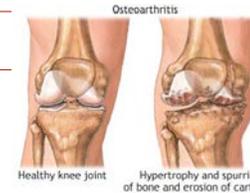
hip resurfacing

hip resurfacing is a surgical procedure which has been developed as an intervention alternative to total hip replacement. the potential advantages of hip resurfacing include **less bone removal**, a potentially lower number of hip dislocations due to a relatively larger femoral head size, and possibly easier revision surgery for a subsequent total hip replacement device. the potential disadvantages are femoral neck fractures, asptic loosening, and metal wear.



example - hip replacement

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osteoarthritis

osteoarthritis, also known as degenerative joint disease or osteoarthrosis, is a group of mechanical abnormalities involving degradation of joints, including articular cartilage and subchondral bone. it affects about 27 million people in the united states alone. symptoms may include joint pain, tenderness, stiffness, locking, and sometimes an effusion. a variety of causes, hereditary, developmental, metabolic, and mechanical, may initiate processes leading to loss of cartilage. when bone surfaces become less well protected by cartilage, bone may be exposed and damaged. treatment generally involves a combination of exercise, lifestyle modification, or, in severe cases, surgical joint replacement.



example - osteoarthritis

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Computational modeling of bone density profiles in response to gait: A subject-specific approach

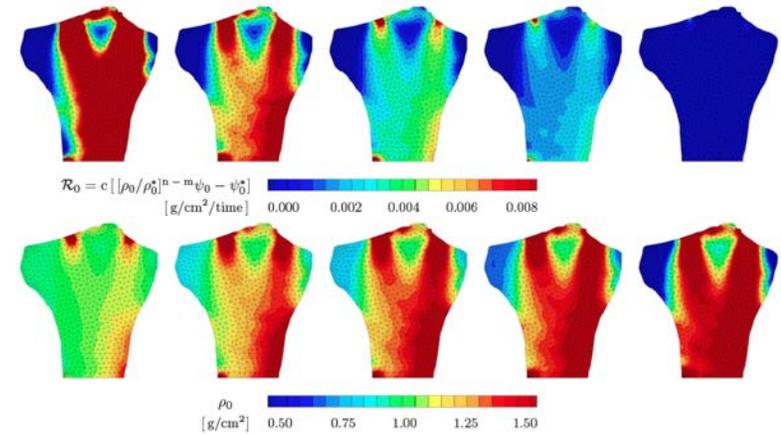
Henry Pang¹, Abhishek P. Shiwalkar¹, Chris M. Madormo¹, Rebecca E. Taylor¹, Thomas P. Andriacchi^{1,2}, Ellen Kuhl^{1,3,4}



pang, shiwalkar, madormo, taylor, andriacchi, kuhl [2012]

example – henry's knee

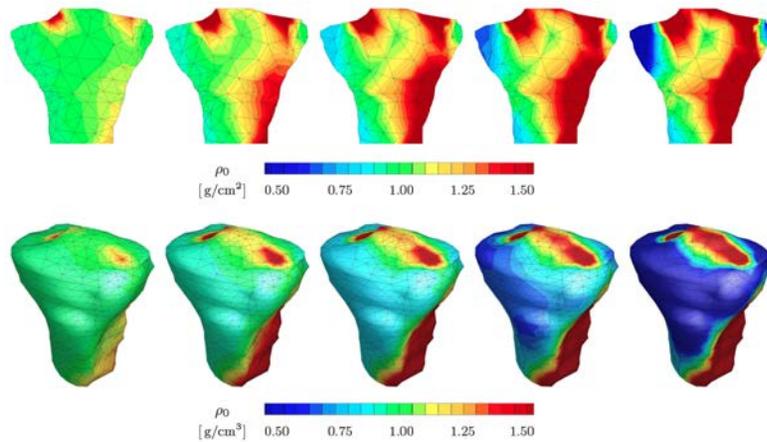
how does henry's bone grow?



pang, shiwalkar, madormo, taylor, andriacchi, kuhl [2012]

example – henry's knee

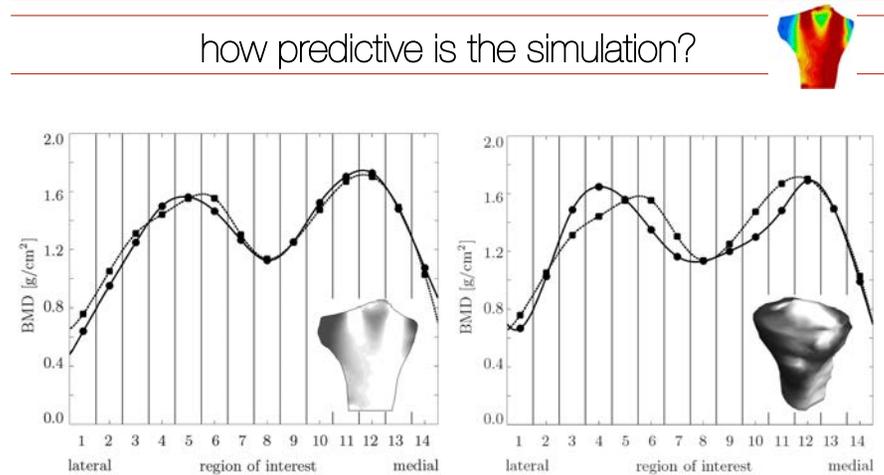
how does henry's bone grow?



pang, shiwalkar, madormo, taylor, andriacchi, kuhl [2012]

example – henry's knee

how predictive is the simulation?



pang, shiwalkar, madormo, taylor, andriacchi, kuhl [2012]

example – henry's knee