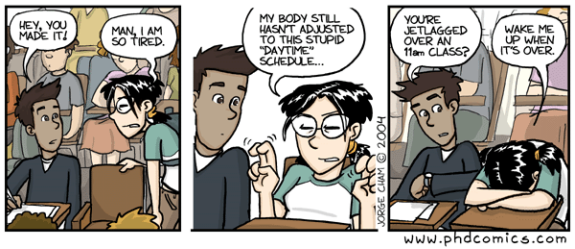
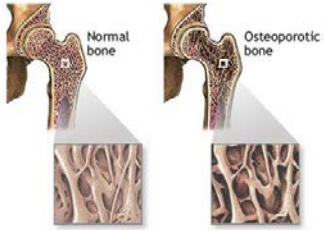
13 - basic constitutive equations - growing bones



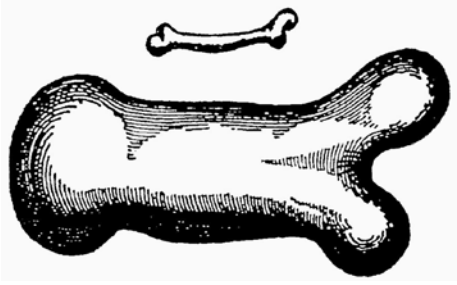
day	date		topic
tue	jan	08	motivation - everything grows!
thu	jan	10	basics maths - notation and tensors
tue	jan	15	basic kinematics - large deformation and growth
thu	jan	17	kinematics - growing hearts
tue	jan	22	guest lecture - growing surfaces
thu	jan	24	kinematics - growing leaflets
tue	jan	29	basic balance equations - closed and open systems
thu	jan	31	basic constitutive equations - growing muscle
tue	feb	05	basic constitutive equations - growing tumors
thu	feb	07	volume growth - finite elements for growth - theory
tue	feb	12	volume growth - finite elements for growth - matlab
thu	feb	14	volume growth - growing skin
tue	feb	19	basic constitutive equations - growing bones
thu	feb	21	density growth - finite elements for growth
tue	feb	26	density growth - growing bones
thu	feb	28	everything grows! - midterm summary
tue	mar	05	midterm
thu	mar	07	remodeling - remodeling arteries and tendons
tue	mar	12	class project - discussion, presentation, evaluation
thu	mar	14	class project - discussion, presentation, evaluation
thu	mar	14	written part of final projects due



osteoporosis

osteoporosis is a disease of bones that leads to an increased risk of fracture. osteoporosis literally means porous bones. in osteoporosis the bone mineral density is reduced, bone microarchitecture is disrupted, and the amount of variety of proteins in bone is altered. the diagnosis of osteoporosis can be made using conventional radiography. bone mineral density can be measured by dual energy x-ray absorptiometry, dxa or dexa. osteoporosis can be prevented with lifestyle changes and sometimes medication. lifestyle changes include exercise and preventing falls, as well as reducing protein intake which may cause calcium to be taken from the bones.

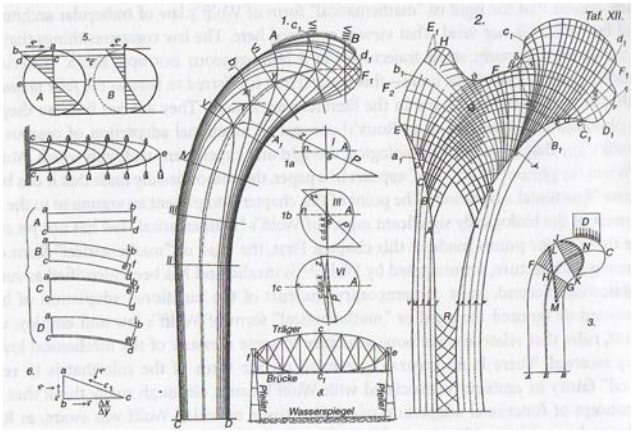
history - 17th century



‚...dal che e manifesto, che chi volesse mantener in un vastissimo gigante le proporzioni, che hanno le membra in un huomo ordinario, bisognerebbe o trouar materia molto piu dura, e resistente per formarne l'ossa o vero ammettere, che la robustezza sua fusse a proporzione assai piu fiacca, che negli huomini de statura mediocre; altrimente crescendogli a smisurata altezza si vedrebbono dal proprio peso opprimere, e cadere…'

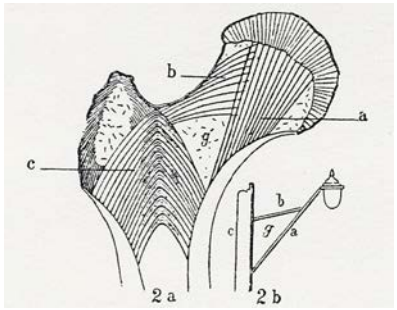
galileo,'discorsi e dimostrazioni matematiche', [1638]

history - 19th century



culmann & von meyer 'graphic statics' [1867]

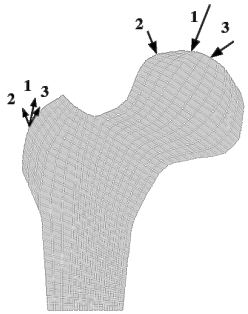
history - 19th century

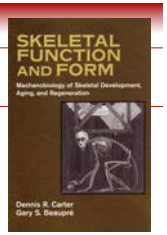


„…es ist demnach unter dem gesetze der transformation der knochen dasjenige gesetz zu verstehen, nach welchem im gefolge primaerer abaenderungen der form und inanspruchnahme bestimmte umwandlungen der inneren architectur und umwandlungen der aeusseren form sich vollziehen..."

wolff 'gesetz der transformation der knochen' [1892]

different load cases

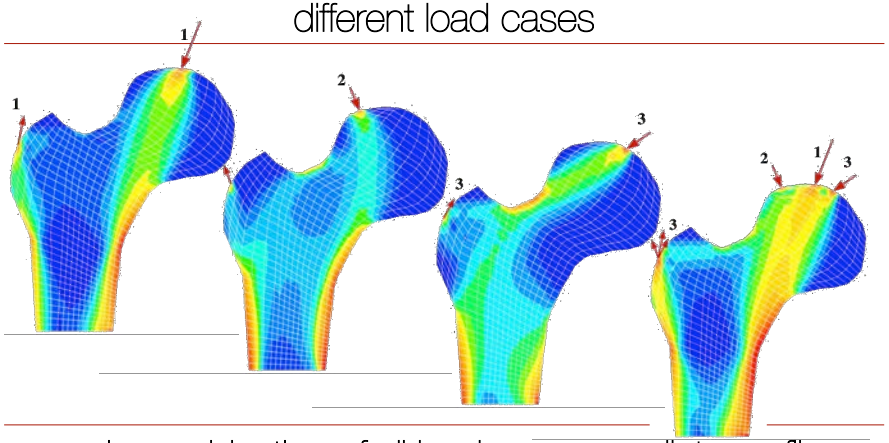




[1]	midstance phase of gait	2317 N	24°	703 N	28°
[2]	extreme range of abduction	1158 N	-15°	351 N	-8 °
[3]	extreme range of adduction	1548 N	56°	468 N	35°

carter & beaupré [2001]

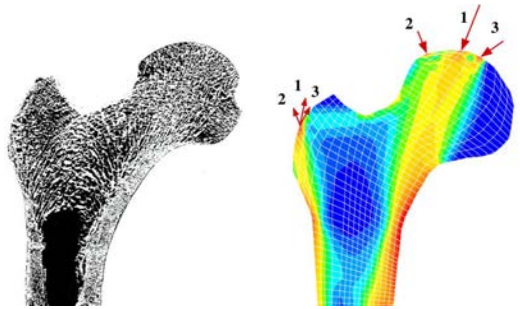
different load cases



only combination of all load cases predicts profile

carter & beaupré [2001]

experiment vs simulation



- dense system of compressive trabaculae carrying stress into calcar region
- secondary arcuate system, medial joint surface to lateral metaphyseal region
- ward ‘s triangle, low density region contrasting dense cortical shaft

carter & beaupré [2001]

motivation - growing bone

class project - me337 - mechanics of growth

rebecca e. taylor

joseph c. doll

amir shamloo

ryan p. jackson

chun hua zheng

nathaniel a. benz

neuromuscular biomechanics lab

scott delp

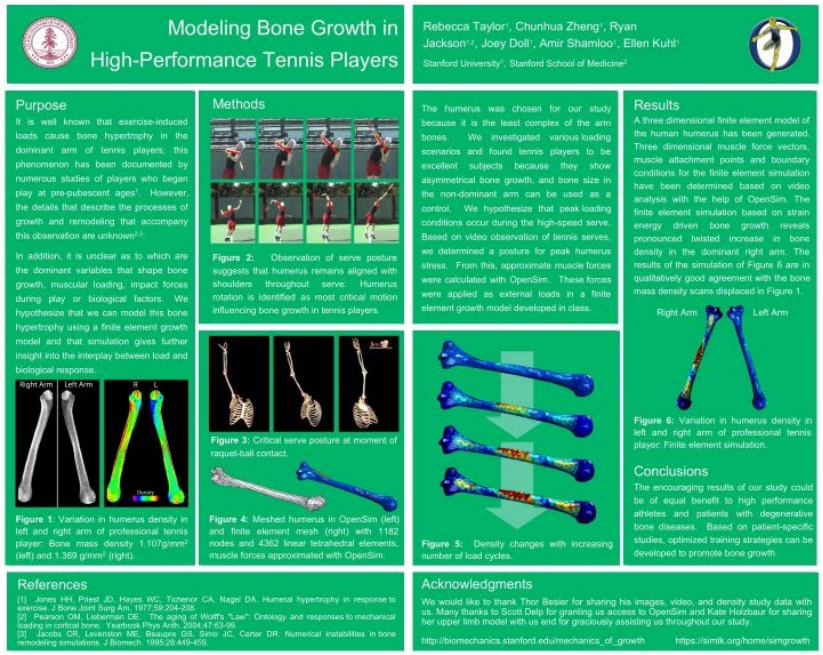
kate holzbaur

human performance lab

thor bezier

inter-arm asymmetry in high performance tennis players

example - twisted tennis arm density



Modeling Bone Growth in High-Performance Tennis Players

Rebecca Taylor[1], Chunhua Zheng[1], Ryan Jackson[1,2], Joey Doll[1], Amir Shamloo[1], Ellen Kuhl[1]

Stanford University[1], Stanford School of Medicine[2]

Purpose

It is well known that exercise-induced loads cause bone hypertrophy in the dominant arm of tennis players; this phenomenon has been documented by numerous studies of players who began play at pre-pubescent ages[1]. However, the details that describe the processes of growth and remodeling that accompany this observation are unknown[2,3].

In addition, it is unclear as to which are the dominant variables that shape bone growth, muscular loading, impact forces during play or biological factors. We hypothesize that we can model this bone hypertrophy using a finite element growth model and that simulation gives further insight into the interplay between load and biological response.

Methods

Figure 2: Observation of serve posture suggests that humerus remains aligned with shoulders throughout serve: Humerus rotation is identified as most critical motion influencing bone growth in tennis players.

Figure 3: Critical serve posture at moment of racquet-ball contact.

Figure 4: Meshed humerus in OpenSim (left) and finite element mesh (right) with 1182 nodes and 4362 linear tetrahedral elements, muscle forces approximated with OpenSim.

The humerus was chosen for our study because it is the least complex of the arm bones. We investigated various loading scenarios and found tennis players to be excellent subjects because they show asymmetrical bone growth, and bone size in the non-dominant arm can be used as a control. We hypothesize that peak loading conditions occur during the high-speed serve. Based on video observation of tennis serves, we determined a posture for peak humerus stress. From this, approximate muscle forces were calculated with OpenSim. These forces were applied as external loads in a finite element growth model developed in class.

Figure 5: Density changes with increasing number of load cycles.

Results

A three dimensional finite element model of the human humerus has been generated. Three dimensional muscle force vectors, muscle attachment points and boundary conditions for the finite element simulation have been determined based on video analysis with the help of OpenSim. The finite element simulation based on strain energy driven bone growth reveals pronounced twisted increase in bone density in the dominant right arm. The results of the simulation of Figure 6 are in qualitatively good agreement with the bone mass density scans displaced in Figure 1.

Figure 6: Variation in humerus density in left and right arm of professional tennis player: Finite element simulation.

Conclusions

The encouraging results of our study could be of equal benefit to high performance athletes and patients with degenerative bone diseases. Based on patient-specific studies, optimized training strategies can be developed to promote bone growth.

References

[1] Jones HH, Priest JD, Hayes WC, Tichenor CA, Nagel DA. Humeral hypertrophy in response to exercise. J Bone Joint Surg Am. 1977;59:204-208.
[2] Pearson OM, Lieberman DE. The aging of Wolff's "Law": Ontology and responses to mechanical loading in cortical bone. Yearbook Phys Anth. 2004;47:63-99.
[3] Jacobs CR, Levenston ME, Beaupre GS, Simo JC, Carter DR. Numerical instabilities in bone remodeling simulations. J Biomech. 1995;28:449-459.

Acknowledgments

We would like to thank Thor Besier for sharing his images, video, and density study data with us. Many thanks to Scott Delp for granting us access to OpenSim and Kate Holzbaur for sharing her upper limb model with us and for graciously assisting us throughout our study.

http://biomechanics.stanford.edu/mechanics_of_growth https://simtk.org/home/simgrowth

example - twisted tennis arm density

The phenomenon of twisted growth: humeral torsion in dominant arms of high performance tennis players

R.E. Taylor[a], C. Zheng[a], R.P. Jackson[b], J.C. Doll[a], J.C. Chen[b], K.R.S. Holzbaur[c], T. Besier[d] and E. Kuhl[ab]*

[a]*Department of Mechanical Engineering, Stanford University, Stanford, CA, USA;* [b]*Department of Bioengineering, Stanford University, Stanford, CA, USA;* [c]*Department of Biomedical Engineering, Wake Forest University School of Medicine, Winston-Salem, NC, USA;* [d]*Department of Orthopaedic Surgery, Stanford University, Stanford, CA, USA*

(*Received 27 November 2007; final version received 2 May 2008*)

This manuscript is driven by the need to understand the fundamental mechanisms that cause twisted bone growth and shoulder pain in high performance tennis players. Our ultimate goal is to predict bone mass density in the humerus through computational analysis. The underlying study spans a unique four level complete analysis consisting of a high-speed video analysis, a musculoskeletal analysis, a finite element based density growth analysis and an X-ray based bone mass density analysis. For high performance tennis players, critical loads are postulated to occur during the serve. From high-speed video analyses, the serve phases of maximum external shoulder rotation and ball impact are identified as most critical loading situations for the humerus. The corresponding posts from the video analysis are reproduced with a musculoskeletal analysis tool to determine muscle attachment points, muscle force vectors and overall forces of relevant muscle groups. Collective representative muscle forces of the deltoid, latissimus dorsi, pectoralis major and triceps are then applied as external loads in a fully 3D finite element analysis. A problem specific nonlinear finite element based density analysis tool is developed to predict functional adaptation over time. The density profiles in response to the identified critical muscle forces during serve are qualitatively compared to X-ray based bone mass density analyses.

Keywords: bone mass density changes; functional adaptation; musculoskeletal analysis; finite element analysis; sports medicine

The Stanford Daily

An Independent Publication

If there's one thing that's guaranteed, it's that Jeff Zeller strives to apply what he knows in various contexts. Whether it be while injured, in doubles or in singles matches, the sophomore will take his wisdom and work to develop his game.

Although the Zeller redshirted in 2006 because of injury, he was still able to observe his teammates in action and apply this knowledge to his own game when he returned to the court.

This year, Zeller has used this experience, and along with senior Eric McKean, has formed a successful doubles pair that draws inspiration from the Bryan brothers (Bob and Mike Bryan — both former Stanford players).

Throughout this season, Zeller has learned to apply doubles tactics in order to improve his singles game, too. These circumstances demonstrate why head coach John Whitlinger will attest to the fact that the Centennial, Colo. native is such a "good student of the game."

Zeller injured his hand in January of 2006 and took three months off from tennis. Even when Zeller started hitting again in the spring, he was not at 100 percent and, therefore, could not practice with the team. In his first year on The Farm, Zeller was forced into the role of an onlooker and was not able to contribute to the team on the court.

Stanford Daily File Photo

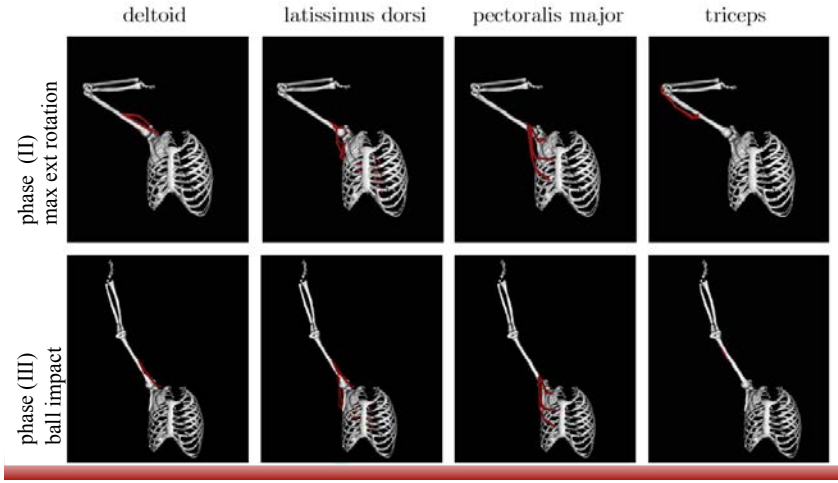
Jeff Zeller / SO

"When I got injured, I took on more of the observer role, but I got to watch my teammates succeed," Zeller said. "I got to watch [sophomore] Matt [Bruch] get ranked top 5 in the country; I got to watch KC [Corkery] get to the semifinals of NCAAs; I got to watch KC and [then-senior] James Pade play some amazing doubles. I think I really learned a lot from just sitting back and seeing what my teammates did well that allowed them to be successful.

example - twisted tennis arm density 13

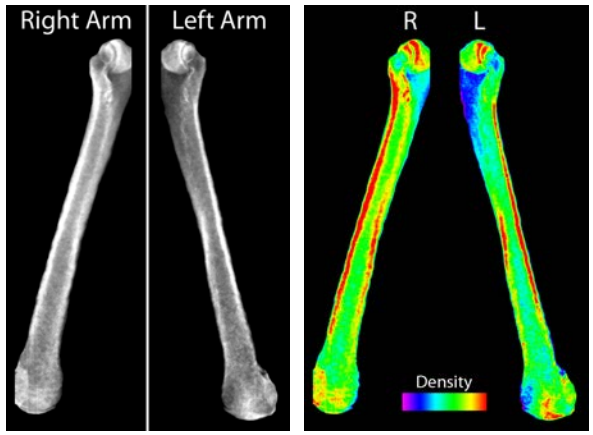
example - twisted tennis arm density 14

critical muscle forces during serve



example - twisted tennis arm density 15

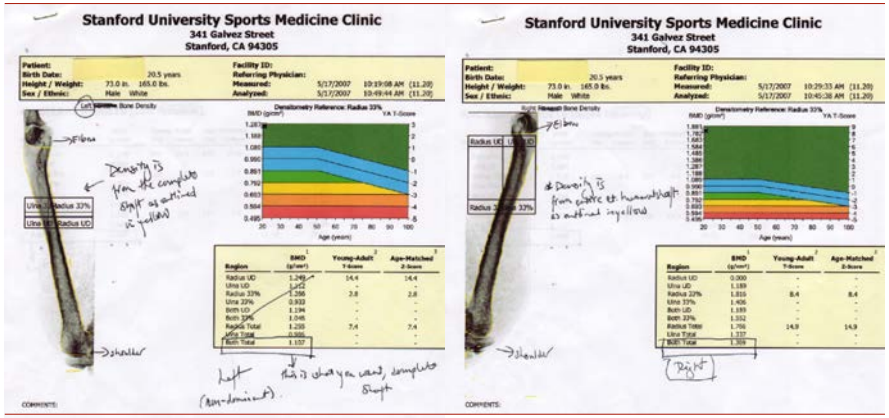
inter-arm asymmetry in bone density



thor besier - human performance lab - stanford

example - twisted tennis arm density 16

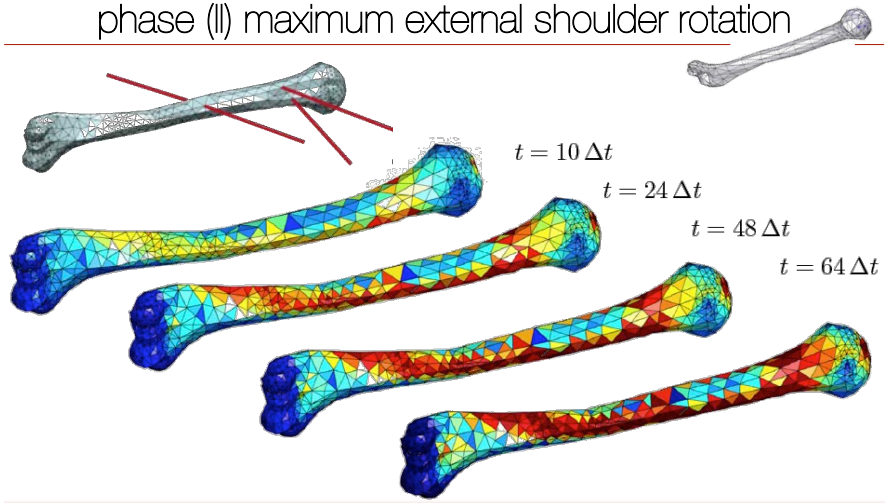
inter-arm asymmetry in bone density



bmd left 1.107g/mm^2 bmd right 1.369g/mm^2

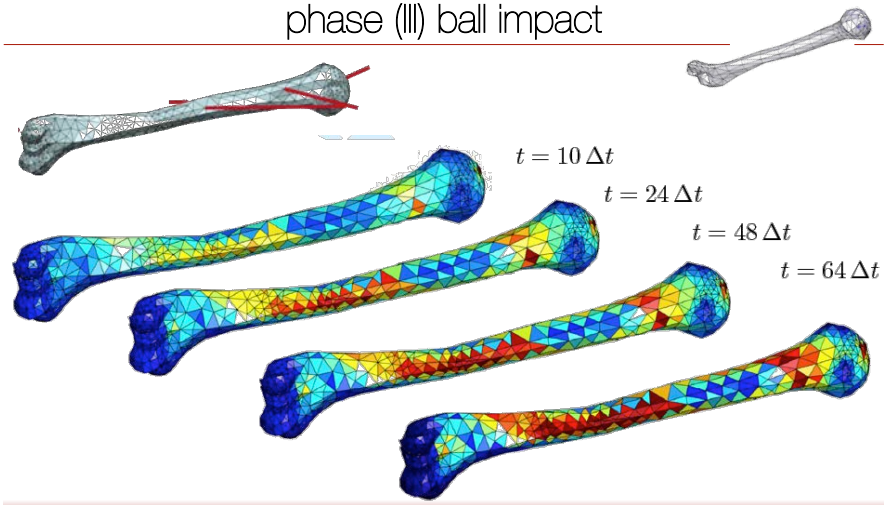
example - twisted tennis arm density 17

phase (II) maximum external shoulder rotation



example - twisted tennis arm density 18

phase (III) ball impact



example - twisted tennis arm density 19

pitcher's arm

a physical-conditioning program for pitchers is geared to striking a balance between muscle strength and endurance, tendon/ligament strength and flexibility, and optimal cartilage and **bone density**. bone hypertrophy occurs in response to physical activity. the bones in the throwing arm of a baseball pitcher are **denser and thicker** than those of the other arm. bone hypertrophy is **stimulated by the magnitude of loading** rather than by the frequency.

example – pitcher's arm 20

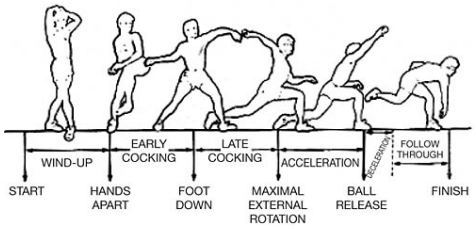
pitcher's arm

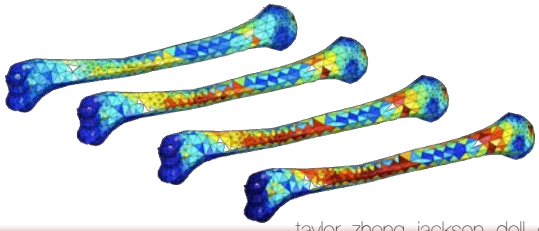
the real secret to tim lincecum's overpowering velocity is all **stored within his pitching mechanics**. it has little to do with his size and strength. six things in tim lincecum's pitching delivery create his amazing arm speed:

- move fast from back leg to front leg
- use back leg to move out very low to ground
- get throwing arm up very late in delivery
- stride length of over 100% of pitcher's height
- brace front leg to increase upper body speed
- land in a straight line toward plate

tim lincecum's pitching mechanics, because he moves fast into a long stride and stays low, forces his body to **put as many muscles on stretch as quickly as possible** which helps develop **maximum elastic energy** so that **his body acts like a huge rubber band** stretching to it's maximum length ready to be let go and whip the arm through.

pitcher's arm

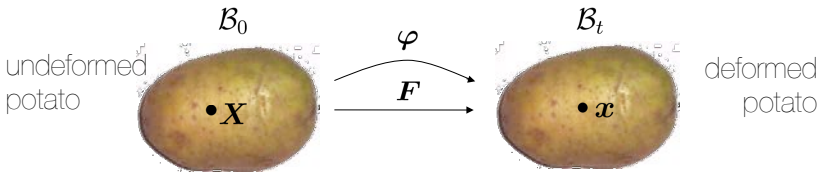




maximal external shoulder rotation stimulates twisted density growth

taylor, zheng, jackson, doll, chen, holzbaur, besier, kuhl [2009]

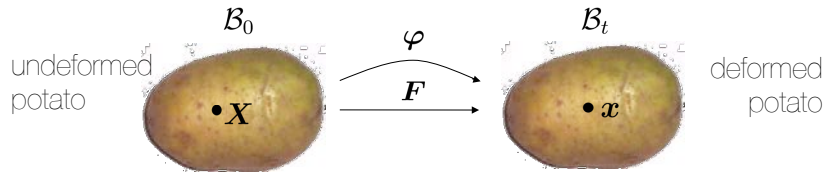
neo hooke'ian elasticity of solid materials



undeformed potato — deformed potato

- free energy $\psi_0^{\text{neo}} = \frac{1}{2}\lambda_0 \ln^2(\det(\boldsymbol{F})) + \frac{1}{2}\mu_0[\boldsymbol{F}^{\text{t}} \cdot \boldsymbol{F} : \boldsymbol{I} - n^{\text{dim}} - 2\ln(\det(\boldsymbol{F}))]$
- definition of stress $\boldsymbol{P}^{\text{neo}} = \mathrm{D}_F \psi_0^{\text{neo}} = \mu_0 \boldsymbol{F} + [\lambda_0 \ln(\det(\boldsymbol{F})) - \mu_0]\boldsymbol{F}^{-\text{t}}$

neo hooke'ian elasticity of solid materials



undeformed potato — deformed potato

- free energy $\psi_0^{\text{neo}} = \frac{1}{2}\lambda_0 \ln^2(\det(\boldsymbol{F})) + \frac{1}{2}\mu_0[\boldsymbol{F}^{\text{t}} \cdot \boldsymbol{F} : \boldsymbol{I} - n^{\text{dim}} - 2\ln(\det(\boldsymbol{F}))]$
- large strain - lamé parameters and bulk modulus $\lambda = \frac{E\nu}{[1+\nu][1-2\nu]}$ $\mu = \frac{E}{2[1+\nu]}$ $\kappa = \frac{E}{3[1-2\nu]}$
- small strain – young's modulus and poisson's ratio $E = 3\kappa[1-2\nu]$ $\nu = \frac{3\kappa-2\mu}{2[3\kappa+\mu]}$

neo hooke'ian elasticity of solid materials

- free energy $\psi_0^{\text{neo}} = \frac{1}{2}\lambda_0 \ln^2(\det(\boldsymbol{F})) + \frac{1}{2}\mu_0[\,\boldsymbol{F}^{\text{t}}\cdot\boldsymbol{F} : \boldsymbol{I} - n^{\text{dim}} - 2\ln(\det(\boldsymbol{F}))\,]$
- definition of stress

$$\begin{aligned}\boldsymbol{P}^{\text{neo}} &= \mathrm{D}_F\psi_0^{\text{neo}}\\ &= \tfrac{1}{2}\lambda_0\, 2\ln(\det\boldsymbol{F})\boldsymbol{F}^{-\text{t}} + \tfrac{1}{2}\mu_0\, 2\,\boldsymbol{F} - \mu_0\boldsymbol{F}^{-\text{t}}\\ &= \mu_0\,\boldsymbol{F} + [\,\lambda_0\ln(\det(\boldsymbol{F})) - \mu_0\,]\boldsymbol{F}^{-\text{t}}\end{aligned}$$

- definition of tangent operator

$$\begin{aligned}\mathbf{A}^{\text{neo}} &= \mathrm{D}_{FF}\psi_0^{\text{neo}} = \mathrm{D}_F\boldsymbol{P}^{\text{neo}}\\ &= \lambda_0\boldsymbol{F}^{-\text{t}}\otimes\boldsymbol{F}^{-\text{t}} + \mu_0\boldsymbol{I}\overline{\otimes}\boldsymbol{I}\\ &\quad +[\mu_0 - \lambda_0\ln(\det(\boldsymbol{F}))]\,\boldsymbol{F}^{-\text{t}}\underline{\otimes}\boldsymbol{F}^{-1}\end{aligned}$$

neo hooke'ian elasticity of solid materials

- free energy $\psi_0^{\text{neo}} = \frac{1}{2}\lambda_0 \ln^2(\det(F_{ij})) + \frac{1}{2}\mu_0[\,F_{ij}F_{ij} - n^{\text{dim}} - 2\ln(\det(F_{ij}))\,]$
- definition of stress

$$\begin{aligned}P_{ij}^{\text{neo}} &= \mathrm{D}_{F_{ij}}\psi_0^{\text{neo}}\\ &= \tfrac{1}{2}\lambda_0\, 2\ln(\det F_{ij})F_{ji}^{-1} + \tfrac{1}{2}\mu_0\, 2\,F_{ij} - \mu_0 F_{ji}^{-1}\\ &= \mu_0\,F_{ij} + [\,\lambda_0\ln(\det(F_{ij})) - \mu_0\,]F_{ji}^{-1}\end{aligned}$$

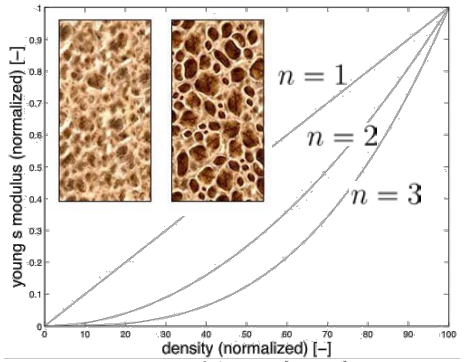
- definition of tangent operator

$$\begin{aligned}\mathsf{A}_{ijkl}^{\text{neo}} &= \mathrm{D}_{F_{ij}F_{kl}}\psi_0^{\text{neo}} = \mathrm{D}_{F_{kl}}P_{ij}^{\text{neo}}\\ &= \lambda_0 F_{ji}^{-1}\,F_{lk}^{-1} + \mu_0 I_{ik}\,I_{jl}\\ &\quad +[\mu_0 - \lambda_0\ln(\det(F_{ij}))]\,F_{li}^{-1}\,F_{jk}^{-1}\end{aligned}$$

neo hooke'ian elasticity of cellular materials

free energy $\psi_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^n \psi_0^{\text{neo}}(\boldsymbol{F})$

$\mathrm{E} = 3.790\ \rho_0^3$ MPa $\quad \rho_0$ in g/cm^3



carter & hayes [1977]

open systems - balance of mass

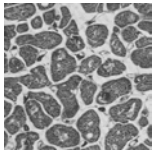
$$\mathrm{D}_t\rho_0 = \mathrm{Div}(\boldsymbol{R}) + \mathcal{R}_0$$

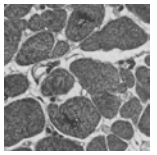
mass flux $\boldsymbol{R}$

- cell movement (migration)

mass source $\mathcal{R}_0$

- cell growth (proliferation)
- cell division (hyperplasia)
- cell enlargement (hypertrophy)





biological equilbrium

cowin & hegedus [1976], beaupré, orr & carter [1990], harrigan & hamilton [1992], jacobs,levenston,beaupré,simo & carter [1995], huiskes [2000], carter & beaupré [2001]

open systems - balance of momentum

- volume specific version

$$\mathrm{D}_t(\rho_0 \boldsymbol{v}) = \mathrm{Div}(\boldsymbol{P} + \boldsymbol{v} \otimes \boldsymbol{R}) + [\boldsymbol{b}_0 + \boldsymbol{v}\mathcal{R}_0 - \nabla_X \boldsymbol{v} \cdot \boldsymbol{R}]$$

- subraction of weighted balance of mass

$$\boldsymbol{v}\,\mathrm{D}_t\rho_0 = \mathrm{Div}(\boldsymbol{v} \otimes \boldsymbol{R}) + \boldsymbol{v}\mathcal{R}_0 - \nabla_X \boldsymbol{v} \cdot \boldsymbol{R}$$

- mass specific version

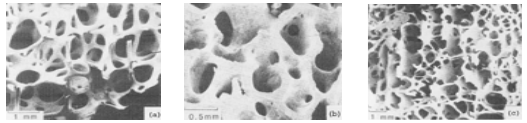
$$\rho_0\,\mathrm{D}_t\boldsymbol{v} = \mathrm{Div}(\boldsymbol{P}) + \boldsymbol{b}_0$$

mechanical equilbrium

balance equations 29

density growth at constant volume

- free energy $\psi_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^n \psi_0^{\mathrm{neo}}(\boldsymbol{F})$
- stress $\boldsymbol{P} = \left[\frac{\rho_0}{\rho_0^*}\right]^n \boldsymbol{P}^{\mathrm{neo}}(\boldsymbol{F})$
- mass flux $\boldsymbol{R} = R_0\,\nabla_X \rho_0$
- mass source $\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m} \psi_0(\boldsymbol{F}) - \psi_0^*$

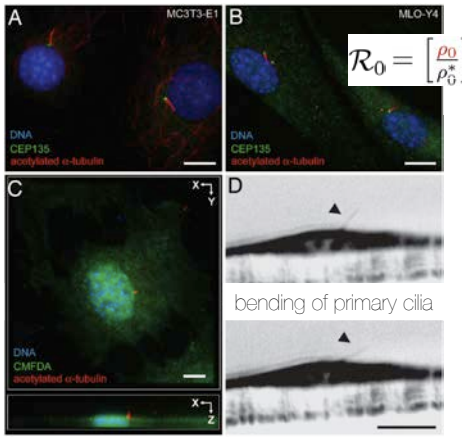


constitutive coupling of growth and deformation

gibson & ashby [1999]

constitutive equations 30

driving force for density growth - why does bone grow?



$$\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m} \psi_0(\boldsymbol{F}) - \psi_0^*$$

energy driven

mechanotransduction

bending of primary cilia

shear stress driven

malone, anderson, tummala, kwon, johnston, stearns, jacobs [2007]

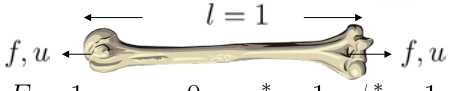
constitutive equations 31

density growth - mass source

$\mathrm{D}_t\rho_0 = \mathcal{R}_0$

1d model problem

$\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m} \psi_0 - \psi_0^*$



$E = 1 \quad \nu = 0 \quad \rho_0^* = 1 \quad \psi_0^* = 1$

$n = 2$
$m = 3$

gradually increased workout

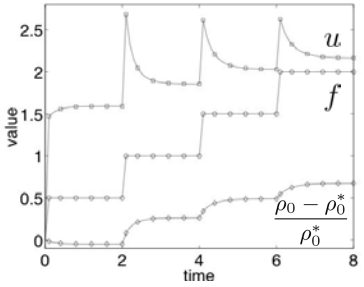
$0 < t \le 2 : f = 0.5\ \mathrm{N}$
$2 < t \le 4 : f = 1.0\ \mathrm{N}$
$4 < t \le 6 : f = 1.5\ \mathrm{N}$
$6 < t \le 8 : f = 2.0\ \mathrm{N}$

how does the mass source control growth?

constitutive equations 32

density growth - mass source

$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \quad f \leftarrow \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$



$f = 0.5\ \mathrm{N} \quad u = 1.5910\,l$
$f = 1.0\ \mathrm{N} \quad u = 1.8559\,l$
$f = 1.5\ \mathrm{N} \quad u = 2.0310\,l$
$f = 2.0\ \mathrm{N} \quad u = 2.1652\,l$

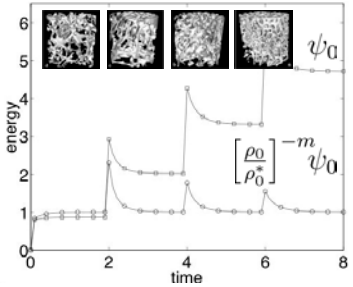
resorption $-1 < \frac{\rho_0-\rho_0^*}{\rho_0^*} < 0$

growth $0 < \frac{\rho_0-\rho_0^*}{\rho_0^*} < \infty$

increasing force causes bone density increase

density growth - mass source

$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \quad f \leftarrow \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$



first time interval $f = 0.5\mathrm{N}$

$u = 1.5910l \quad \varphi = X + u = 2.5910l$

$F = \frac{\partial\varphi}{\partial X} = \frac{\partial\, 2.5910\,l}{\partial l} = 2.5910$ homog.

$E = 1 \quad \lambda_0 = \frac{E\,\nu}{[1+\nu][1-2\,\nu]} = 0$

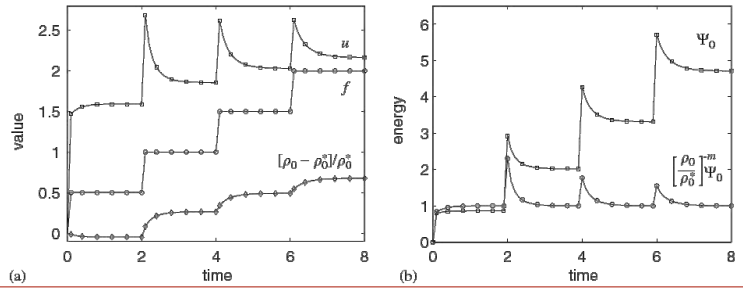
$\nu = 0 \quad \mu_0 = \frac{E}{2\,[1+\nu]} = 0.5$

$\psi_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^n \frac{1}{2}\,\mu_0[\,F^2 - 1 - 2\,\ln(F)\,]$

increasing force causes energy increase

density growth - mass source

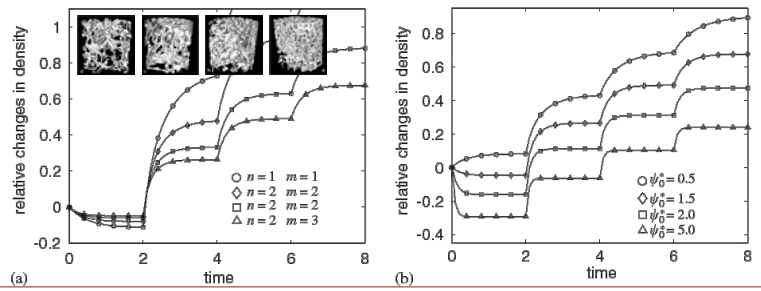
$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \quad f \leftarrow \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$



convergence towards biological equilibrium $\mathrm{D}_t\rho_0 = 0$

density growth - mass source

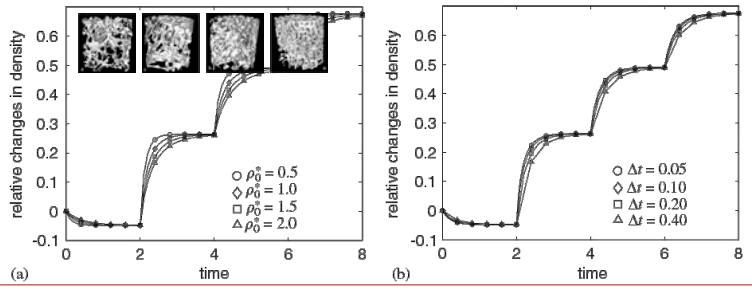
$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \quad f \leftarrow \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$



parameter sensitivity with respect to n, m, ψ_0^*

density growth - mass source

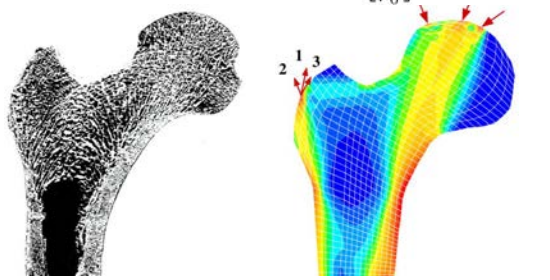
$$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \qquad f \leftarrow \quad \rightarrow f \qquad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$$



parameter insensitivity with respect to $\rho_0^*, \Delta t$

density growth - mass source

$$\mathrm{D}_t\rho_0 = \mathcal{R}_0 \qquad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*}\right]^{-m}\psi_0 - \psi_0^*$$

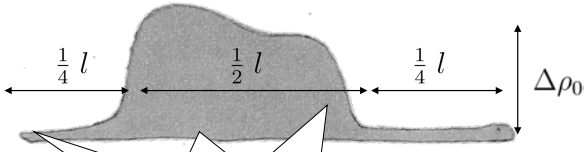


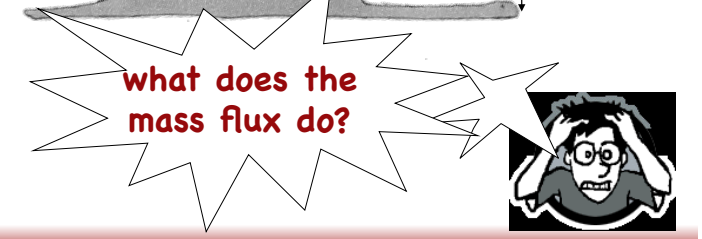
the density evolves such that the tissue can just support the given mechanical load

density growth - mass flux

$$\mathrm{D}_t\rho_0 = \mathrm{Div}(\boldsymbol{R}) \qquad \boldsymbol{R} = R_0\,\nabla_X\rho_0$$

initial hat type density distriubtion

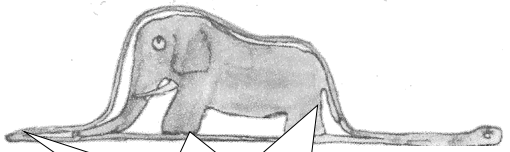


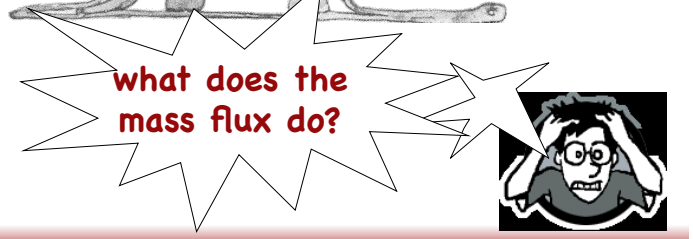


density growth - mass flux

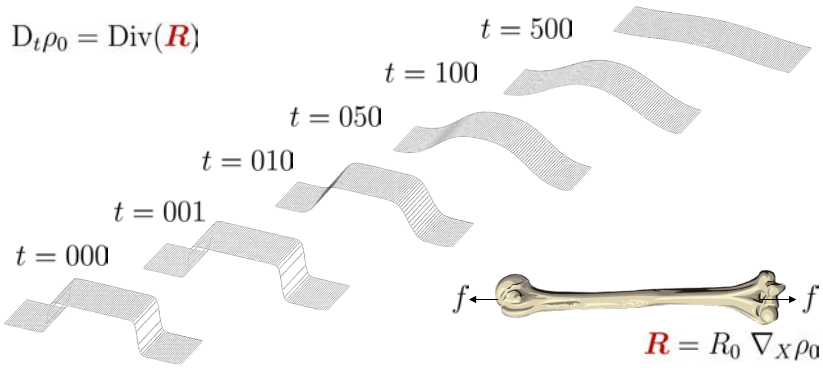
$$\mathrm{D}_t\rho_0 = \mathrm{Div}(\boldsymbol{R}) \qquad \boldsymbol{R} = R_0\,\nabla_X\rho_0$$

initial hat type density distriubtion





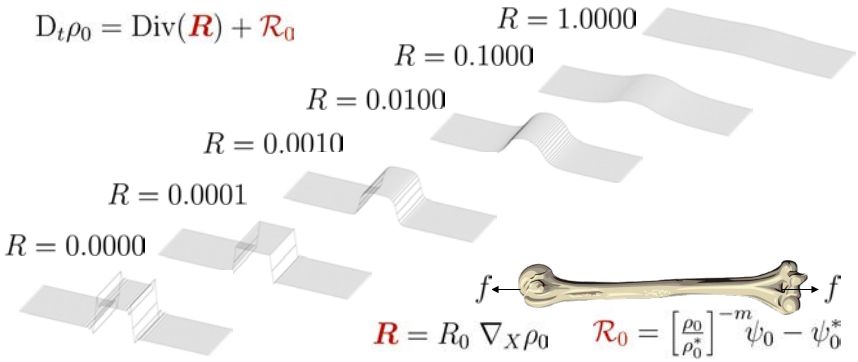
density growth - mass flux



mass flux equilibrates concentrations

constitutive equations 41

density growth - mass flux & source



mass flux smoothens concentration profiles

constitutive equations 42

density growth - bone loss in space

human space flight to mars could become a reality within the next 25 years, but not until some physiological problems are resolved, including an **alarming loss of bone mass, fitness and muscle strength**. gravity at mars' surface is about **38 percent** of that on earth. with lower gravitational forces, **bones decrease in mass and density**. the rate at which we lose bone in space is 10-15 times greater than that of a post-menopausal woman and there is no evidence that bone loss ever slows in space. further, it is not clear that space travelers will regain that bone on returning to gravity. druing a trip to mars, lasting 13 and 30 months, unchecked bone loss could make an astronaut's skeleton the equivalent of a 100-year-old person.

http://www.acsm.org

example - bone loss in space 43

density growth - bone loss in space

$$D_t\rho_0 = \mathcal{R}_0 \qquad \mathcal{R}_0 = c\,\frac{\rho_0}{\psi_0^*}[\psi_0 - \psi_0^*]$$

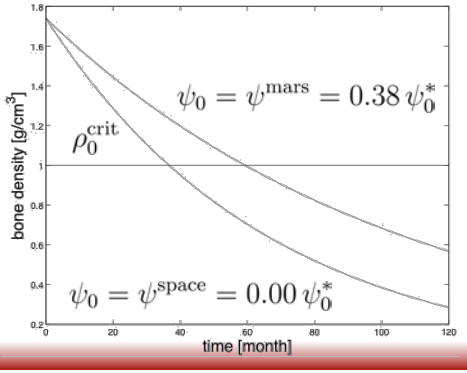
nasa has collected data that humans in space lose bone mass at a rate of $c = 1.5\%/\mathrm{month}$. so far, **no astronauts have been in space for more than 14 months** but the predicted rate of bone loss seems constant in time. this could be a severe problem if we want to send astronauts on a **3 year trip to mars and back**. how long could an astronaut survive in a zero-g environment if we assume the critical bone density to be $\rho_0^{\mathrm{crit}} = 1.00\frac{\mathrm{g}}{\mathrm{cm}^3}$? you can assume an initial density of $\rho_0^* = 1.79\frac{\mathrm{g}}{\mathrm{cm}^3}$!

example - bone loss in space 44

density growth - bone loss in space

$$D_t\rho_0 = c\,\rho_0[\,\tfrac{\psi_0}{\psi_0^*} - 1\,] \qquad D_t\rho_0 = \tfrac{1}{\Delta t}[\rho_0^{n+1} - \rho_0^n]$$

$$\rho_0^{n+1} = \rho_0^n + c\,\rho_0^n[\,\tfrac{\psi_0}{\psi_0^*} - 1\,]\,\Delta t \qquad \rho_0(t_0) = 1.79\tfrac{g}{cm^3}$$



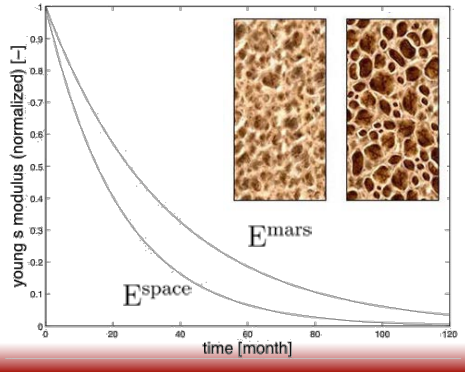
$$\rho_0(36) = 1.0098$$
$$\rho_0(37) = 0.9947$$

example - bone loss in space

density growth - bone loss in space

$$E = 3.790\ \rho_0^3\ \text{MPa} \quad \text{with } \rho_0 \text{ in g/cm}^3$$

carter & hayes [1977]



example - bone loss in space