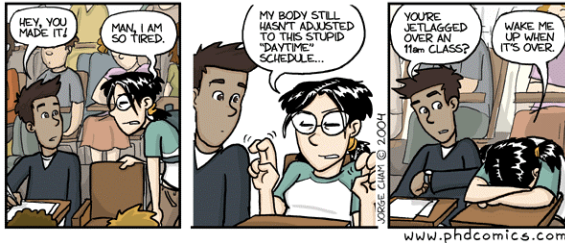


13 - basic constitutive equations - growing bones



13 - constitutive equations

1

day	date	topic
tue	jan 10	motivation - everything grows!
thu	jan 12	basics maths - notation and tensors
tue	jan 17	basic kinematics - large deformation and growth
thu	jan 19	kinematics - growing hearts
tue	jan 24	guest lecture - growing skin
thu	jan 26	guest lecture - growing leaflets
tue	jan 31	basic balance equations - closed and open systems
thu	feb 02	basic constitutive equations - growing tumors
tue	feb 07	volume growth - finite elements for growth
thu	feb 09	volume growth - growing arteries
tue	feb 14	volume growth - growing skin
thu	feb 16	volume growth - growing hearts
tue	feb 21	basic constitutive equations - growing bones
thu	feb 23	density growth - finite elements for growth
tue	feb 28	density growth - growing bones
thu	mar 01	everything grows! - midterm summary
tue	mar 06	midterm
thu	mar 08	remodeling - remodeling arteries and tendons
tue	mar 13	class project - discussion, presentation, evaluation
thu	mar 15	class project - discussion, presentation, evaluation
thu	mar 15	written part of final projects due

where are we???

2



osteoporosis

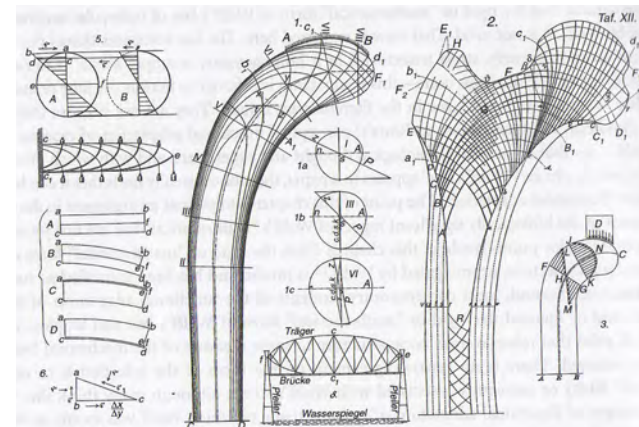
osteoporosis is a disease of bones that leads to an increased risk of fracture. osteoporosis literally means porous bones. in osteoporosis the bone mineral density is reduced, bone microarchitecture is disrupted, and the amount of variety of proteins in bone is altered. the diagnosis of osteoporosis can be made using conventional radiography. bone mineral density can be measured by dual energy x-ray absorptiometry, dxa or dexa. osteoporosis can be prevented with lifestyle changes and sometimes medication. lifestyle changes include exercise and preventing falls. as well as reducing protein intake which may cause calcium to be taken from the bones.



motivation - growing bone

3

history - 19th century

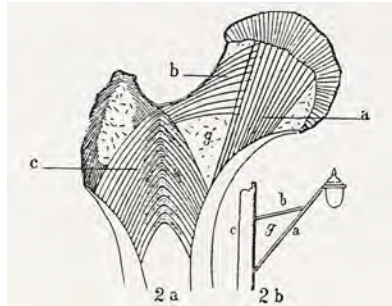


culmann & von meyer "graphic statics" [1867]

motivation - growing bone

4

history - 19th century



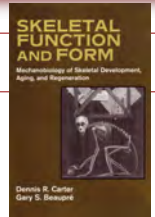
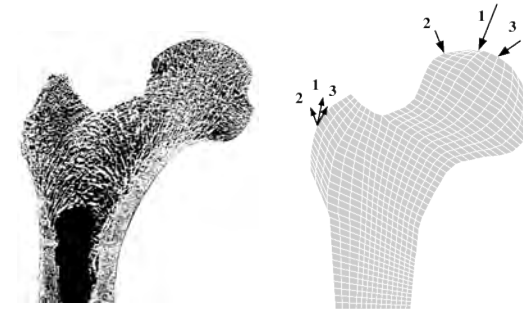
„...es ist demnach unter dem gesetze der transformation der knochen dasjenige gesetz zu verstehen, nach welchem im gefolge primaerer abaenderungen der form und inanspruchnahme bestimmte umwandlungen der inneren architectur und umwandlungen der aeuusseren form sich vollziehen...“

woelf "gesetz der transformation der knochen" [1892]

motivation - growing bone

5

different load cases



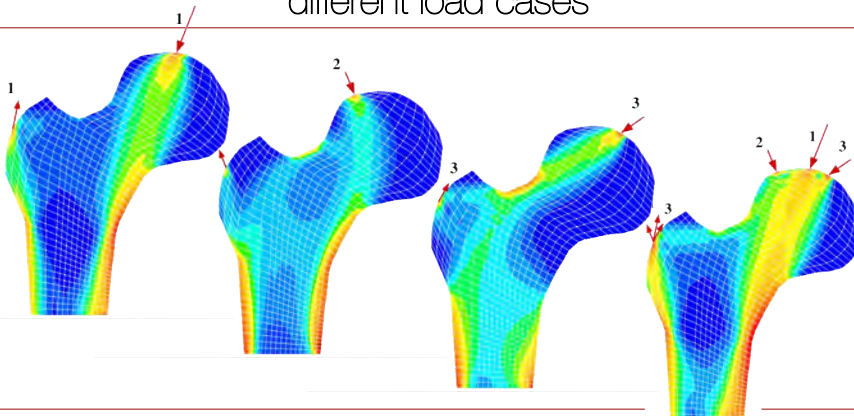
[1] midstance phase of gait	2317 N	24°	703 N	28°
[2] extreme range of abduction	1158 N	-15°	351 N	-8°
[3] extreme range of adduction	1548 N	56°	468 N	35°

carter & beaupré [2001]

motivation - growing bone

6

different load cases



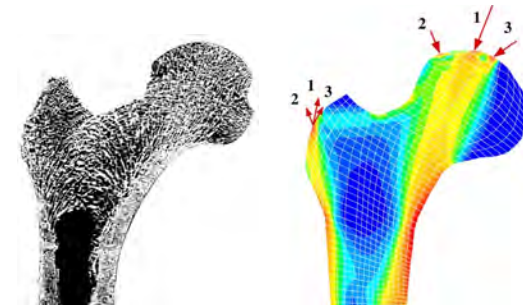
only combination of all load cases predicts profile

carter & beaupré [2001]

motivation - growing bone

7

experiment vs simulation

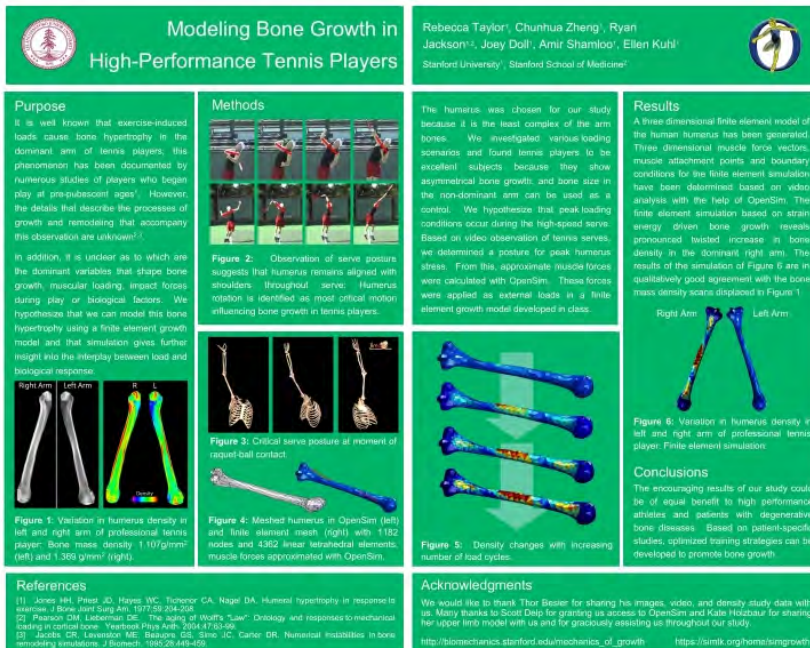


- **dense system of compressive trabeculae** carrying stress into calcar region
- **secondary arcuate system**, medial joint surface to lateral metaphyseal region
- **ward's triangle**, low density region contrasting **dense cortical shaft**

carter & beaupré [2001]

motivation - growing bone

8



class project - me337 - mechanics of growth

rebecca e. taylor
joseph c. doll
amir shamloo
ryan p. jackson
chun hua zheng
nathaniel a. benz

neuromuscular
biomechanics lab
scott delp
kate holzbaur
human
performance lab
thor bezier



inter-arm asymmetry in high performance tennis players

example - twisted tennis arm density

10

The Stanford Daily

An Independent Publication

If there's one thing that's guaranteed, it's that Jeff Zeller strives to apply what he knows in various contexts. Whether it be while injured, in doubles or in singles matches, the sophomore will take his wisdom and work to develop his game.

Although the Zeller redshirted in 2006 because of injury, he was still able to observe his teammates in action and apply this knowledge to his own game when he returned to the court.

This year, Zeller has used this experience, and along with senior Eric McKean, has formed a successful doubles pair that draws inspiration from the Bryan brothers (Bob and Mike Bryan — both former Stanford players).

Throughout this season, Zeller has learned to apply doubles tactics in order to improve his singles game, too. These circumstances demonstrate why head coach John Whitlinger will attest to the fact that the Centennial, Colo. native is such a "good student of the game."

Zeller injured his hand in January of 2006 and took three months off from tennis. Even when Zeller started hitting again in the spring, he was not at 100 percent and, therefore, could not practice with the team. In his first year on The Farm, Zeller was forced into the role of an onlooker and was not able to contribute to the team on the court.

"When I got injured, I took on more of the observer role, but I got to watch my teammates succeed," Zeller said. "I got to watch [sophomore] Matt [Bruch] get ranked top 5 in the country; I got to watch KC [Corkery] get to the semifinals of NCAAs; I got to watch KC and [then-senior] James Pade play some amazing doubles. I think I really learned a lot from just sitting back and seeing what my teammates did well that allowed them to be successful."



Jeff Zeller / SO

example - twisted tennis arm density

11

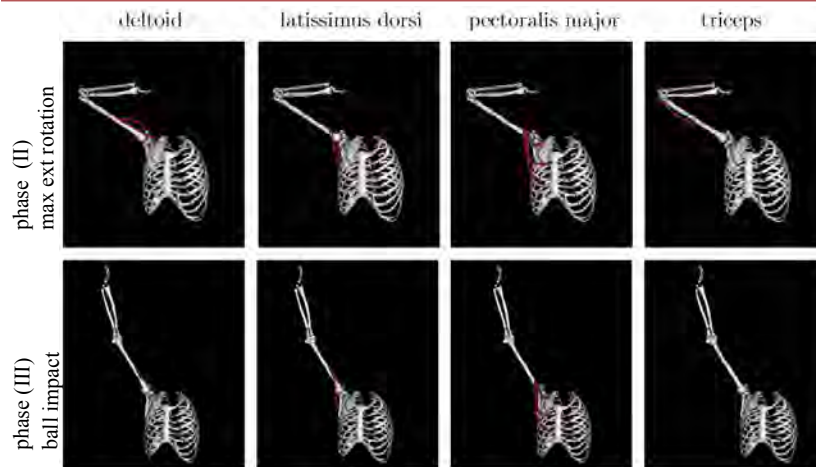
phase (I) backswing
phase (II) max ext rotation
phase (III) ball impact
phase (IV) max int rotation



example - twisted tennis arm density

12

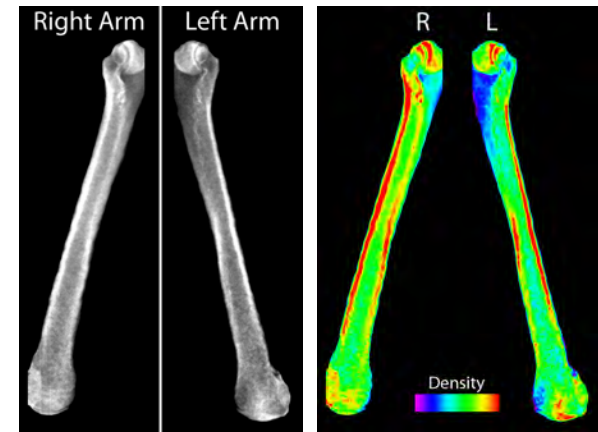
critical muscle forces during serve



example - twisted tennis arm density

13

inter-arm asymmetry in bone density

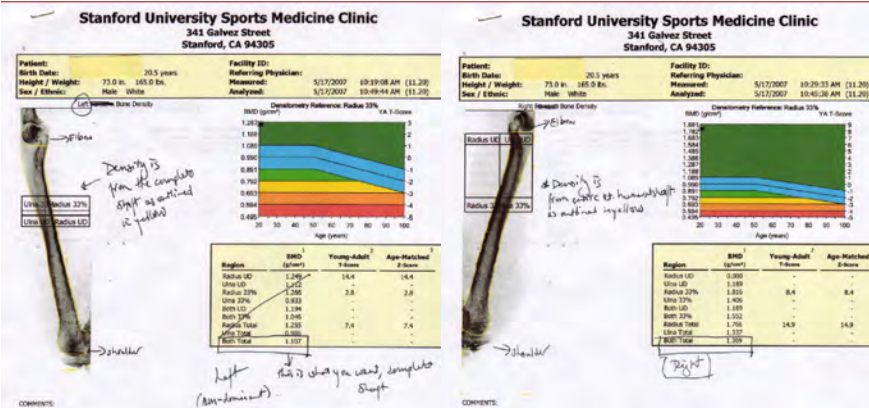


thor besier - human performance lab - stanford

example - twisted tennis arm density

14

inter-arm asymmetry in bone density



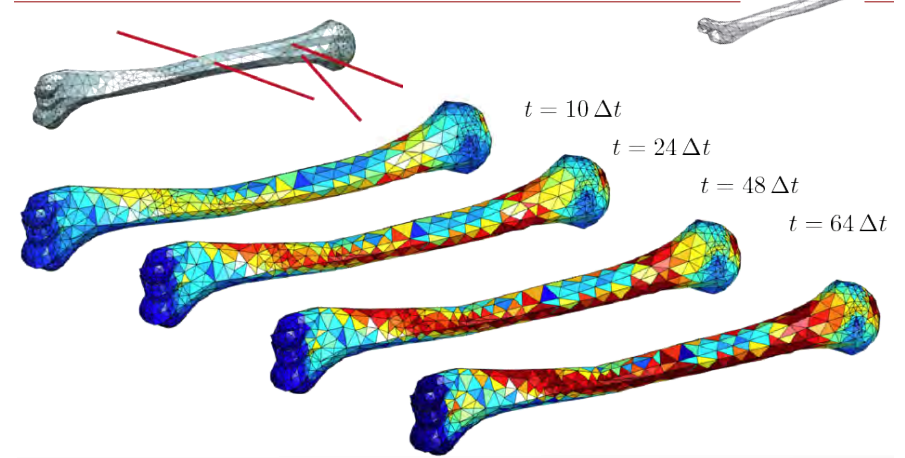
bmd left 1.107g/mm²

bmd right 1.369g/mm²

example - twisted tennis arm density

15

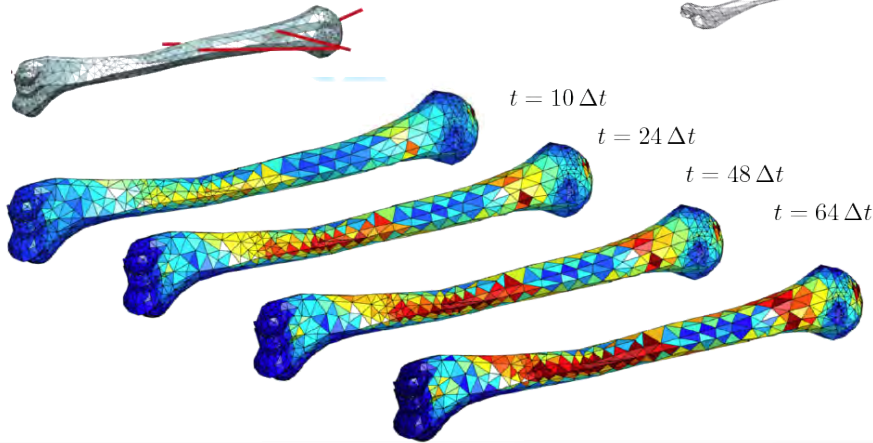
phase (II) maximum external shoulder rotation



example - twisted tennis arm density

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phase (III) ball impact



example - twisted tennis arm density

17

The phenomenon of twisted growth: humeral torsion in dominant arms of high performance tennis players

R.E. Taylor^a, C. Zheng^a, R.P. Jackson^b, J.C. Doll^a, J.C. Chen^b, K.R.S. Holzbaur^c, T. Besier^d and E. Kuhl^{ab*}

^aDepartment of Mechanical Engineering, Stanford University, Stanford, CA, USA; ^bDepartment of Bioengineering, Stanford University, Stanford, CA, USA; ^cDepartment of Biomedical Engineering, Wake Forest University School of Medicine, Winston-Salem, NC, USA; ^dDepartment of Orthopaedic Surgery, Stanford University, Stanford, CA, USA

(Received 27 November 2007; final version received 2 May 2008)

This manuscript is driven by the need to understand the fundamental mechanisms that cause twisted bone growth and shoulder pain in high performance tennis players. Our ultimate goal is to predict bone mass density in the humerus through computational analysis. The underlying study spans a unique four level complete analysis consisting of a high-speed video analysis, a musculoskeletal analysis, a finite element based density growth analysis and an X-ray based bone mass density analysis. For high performance tennis players, critical loads are postulated to occur during the serve. From high-speed video analyses, the serve phases of maximum external shoulder rotation and ball impact are identified as most critical loading situations for the humerus. The corresponding poses from the video analysis are reproduced with a musculoskeletal analysis tool to determine muscle attachment points, muscle force vectors and overall forces of relevant muscle groups. Collective representative muscle forces of the deltoid, latissimus dorsi, pectoralis major and triceps are then applied as external loads in a fully 3D finite element analysis. A problem specific nonlinear finite element based density analysis tool is developed to predict functional adaptation over time. The density profiles in response to the identified critical muscle forces during serve are qualitatively compared to X-ray based bone mass density analyses.

Keywords: bone mass density changes; functional adaptation; musculoskeletal analysis; finite element analysis; sports medicine

pitcher's arm



a physical-conditioning program for pitchers is geared to striking a balance between muscle strength and endurance, tendon/ligament strength and flexibility, and optimal cartilage and **bone density**. bone hypertrophy occurs in response to physical activity. the bones in the throwing arm of a baseball pitcher are **denser and thicker** than those of the other arm. bone hypertrophy is **stimulated by the magnitude of loading** rather than by the frequency.

example - pitcher's arm

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pitcher's arm

the real secret to tim lincecum's overpowering velocity is all **stored within his pitching mechanics**. it has little to do with his size and strength. six things in tim lincecum's pitching delivery create his amazing arm speed:

- move fast from back leg to front leg
- use back leg to move out very low to ground
- get throwing arm up very late in delivery
- stride length of over 100% of pitcher's height
- brace front leg to increase upper body speed
- land in a straight line toward plate

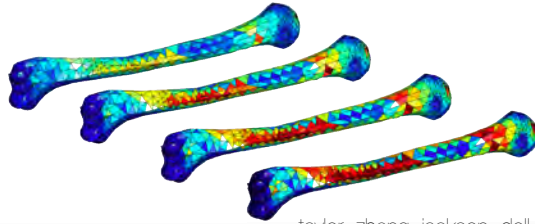
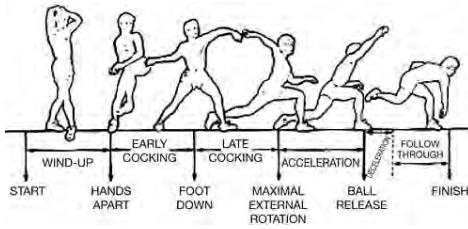


tim lincecum's pitching mechanics, because he moves fast into a long stride and stays low, forces his body to **put as many muscles on stretch as quickly as possible** which helps develop **maximum elastic energy** so that **his body acts like a huge rubber band** stretching to it's maximum length ready to be let go and whip the arm through.

example - pitcher's arm

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pitcher's arm



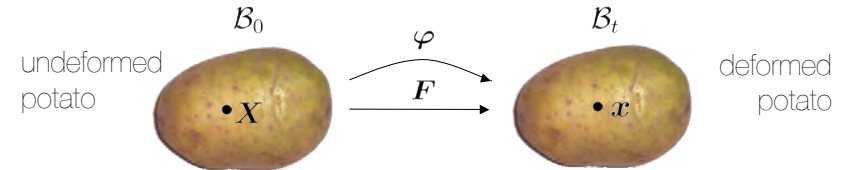
maximal external shoulder rotation stimulates twisted density growth

taylor, zheng, jackson, doll, chen, holzbaun, besier, kuhl [2009]

example - pitcher's arm

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neo hooke'ian elasticity of solid materials

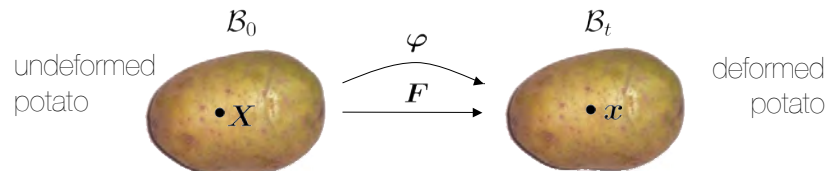


- free energy $\psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 \ln^2(\det(\mathbf{F})) + \frac{1}{2} \mu_0 [\mathbf{F}^t \cdot \mathbf{F} : \mathbf{I} - n^{\text{dim}} - 2 \ln(\det(\mathbf{F}))]$
- definition of stress $\mathbf{P}^{\text{neo}} = D_F \psi_0^{\text{neo}} = \mu_0 \mathbf{F} + [\lambda_0 \ln(\det(\mathbf{F})) - \mu_0] \mathbf{F}^{-t}$

constitutive equations

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neo hooke'ian elasticity of solid materials



- free energy $\psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 \ln^2(\det(\mathbf{F})) + \frac{1}{2} \mu_0 [\mathbf{F}^t \cdot \mathbf{F} : \mathbf{I} - n^{\text{dim}} - 2 \ln(\det(\mathbf{F}))]$
- large strain - lamé parameters and bulk modulus $\lambda = \frac{E\nu}{[1+\nu][1-2\nu]}$ $\mu = \frac{E}{2[1+\nu]}$ $\kappa = \frac{E}{3[1-2\nu]}$
- small strain - young's modulus and poisson's ratio $E = 3\kappa[1-2\nu]$ $\nu = \frac{3\kappa-2\mu}{2[3\kappa+\mu]}$

constitutive equations

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neo hooke'ian elasticity of solid materials

- free energy $\psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 \ln^2(\det(\mathbf{F})) + \frac{1}{2} \mu_0 [\mathbf{F}^t \cdot \mathbf{F} : \mathbf{I} - n^{\text{dim}} - 2 \ln(\det(\mathbf{F}))]$
- definition of stress $\mathbf{P}^{\text{neo}} = D_F \psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 2 \ln(\det \mathbf{F}) \mathbf{F}^{-t} + \frac{1}{2} \mu_0 2 \mathbf{F} - \mu_0 \mathbf{F}^{-t} = \mu_0 \mathbf{F} + [\lambda_0 \ln(\det(\mathbf{F})) - \mu_0] \mathbf{F}^{-t}$
- definition of tangent operator $\mathbf{A}^{\text{neo}} = D_{FF} \psi_0^{\text{neo}} = D_F \mathbf{P}^{\text{neo}} = \lambda_0 \mathbf{F}^{-t} \otimes \mathbf{F}^{-t} + \mu_0 \mathbf{I} \otimes \mathbf{I} + [\mu_0 - \lambda_0 \ln(\det(\mathbf{F}))] \mathbf{F}^{-t} \otimes \mathbf{F}^{-t}$

constitutive equations

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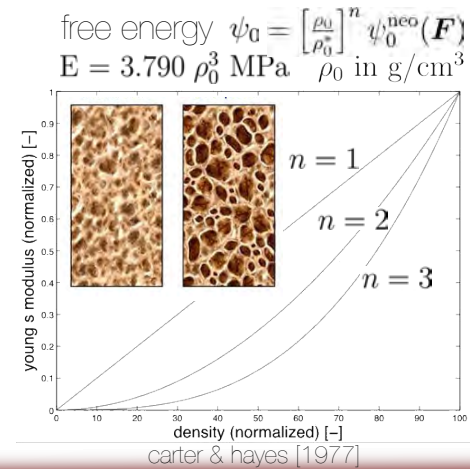
neo hooke'ian elasticity of solid materials

- free energy $\psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 \ln^2(\det(F_{ij})) + \frac{1}{2} \mu_0 [F_{ij} F_{ij} - n^{\text{dim}} - 2 \ln(\det(F_{ij}))]$
- definition of stress $P_{ij}^{\text{neo}} = D_{F_{ij}} \psi_0^{\text{neo}} = \frac{1}{2} \lambda_0 2 \ln(\det F_{ij}) F_{ji}^{-1} + \frac{1}{2} \mu_0 2 F_{ij} - \mu_0 F_{ji}^{-1} = \mu_0 F_{ij} + [\lambda_0 \ln(\det(F_{ij})) - \mu_0] F_{ji}^{-1}$
- definition of tangent operator $A_{ijkl}^{\text{neo}} = D_{F_{ij} F_{kl}} \psi_0^{\text{neo}} = D_{F_{kl}} P_{ij}^{\text{neo}} = \lambda_0 F_{ji}^{-1} F_{lk}^{-1} + \mu_0 I_{ik} I_{jl} + [\mu_0 - \lambda_0 \ln(\det(F_{ij}))] F_{li}^{-1} F_{jk}^{-1}$

constitutive equations

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neo hooke'ian elasticity of cellular materials



constitutive equations

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open systems - balance of mass

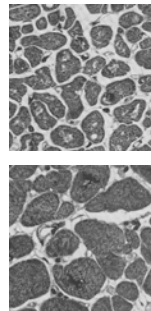
$$D_t \rho_0 = \text{Div}(\mathbf{R}) + \mathcal{R}_0$$

mass flux \mathbf{R}

- cell movement (migration)

mass source \mathcal{R}_0

- cell growth (proliferation)
- cell division (hyperplasia)
- cell enlargement (hypertrophy)



biological equilibrium

cowin & hegedus [1976], beaupré, orr & carter [1990], harrigan & hamilton [1992], jacobs, levenston, beaupré, simo & carter [1995], huiskes [2000], carter & beaupré [2001]

balance equations

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open systems - balance of momentum

- volume specific version

$$D_t(\rho_0 \mathbf{v}) = \text{Div}(\mathbf{P} + \mathbf{v} \otimes \mathbf{R}) + [\mathbf{b}_0 + \mathbf{v} \mathcal{R}_0 - \nabla_X \mathbf{v} \cdot \mathbf{R}]$$

- subtraction of weighted balance of mass

$$\mathbf{v} D_t \rho_0 = \text{Div}(\mathbf{v} \otimes \mathbf{R}) + \mathbf{v} \mathcal{R}_0 - \nabla_X \mathbf{v} \cdot \mathbf{R}$$

- mass specific version

$$\rho_0 D_t \mathbf{v} = \text{Div}(\mathbf{P}) + \mathbf{b}_0$$

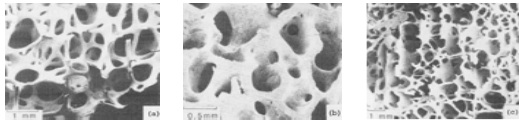
mechanical equilibrium

balance equations

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density growth at constant volume

- free energy $\psi_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^n \psi_0^{\text{neo}}(\mathbf{F})$
- stress $\mathbf{P} = \left[\frac{\rho_0}{\rho_0^*} \right]^n \mathbf{P}^{\text{neo}}(\mathbf{F})$
- mass flux $\mathbf{R} = R_0 \nabla_X \rho_0$
- mass source $\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0(\mathbf{F}) - \psi_0^*$



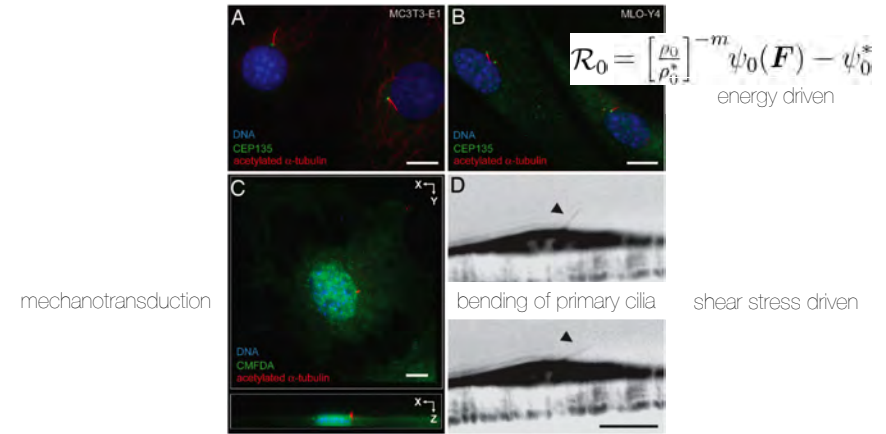
constitutive coupling of growth and deformation

gibson & ashby [1999]

constitutive equations

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driving force for density growth - why does bone grow?



malone, anderson, tummala, kwon, johnston, steams, jacobs [2007]

constitutive equations

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density growth - mass source

$D_t \rho_0 = \mathcal{R}_0$ 1d model problem $\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$

f, u $l = 1$ $n = 2$ $m = 3$

$E = 1$ $\nu = 0$ $\rho_0^* = 1$ $\psi_0^* = 1$

gradually increased workout



$0 < t \leq 2: f = 0.5 \text{ N}$
 $2 < t \leq 4: f = 1.0 \text{ N}$
 $4 < t \leq 6: f = 1.5 \text{ N}$
 $6 < t \leq 8: f = 2.0 \text{ N}$

how does the
mass source control
growth?

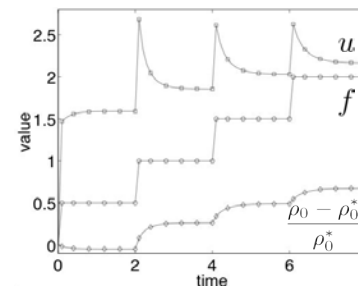


constitutive equations

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density growth - mass source

$D_t \rho_0 = \mathcal{R}_0$ $f \leftarrow$  $\rightarrow f$ $\mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$



$f = 0.5 \text{ N}$ $u = 1.5910 \text{ l}$
 $f = 1.0 \text{ N}$ $u = 1.8559 \text{ l}$
 $f = 1.5 \text{ N}$ $u = 2.0310 \text{ l}$
 $f = 2.0 \text{ N}$ $u = 2.1652 \text{ l}$

resorption $-1 < \frac{\rho_0 - \rho_0^*}{\rho_0^*} < 0$
 growth $0 < \frac{\rho_0 - \rho_0^*}{\rho_0^*} < \infty$

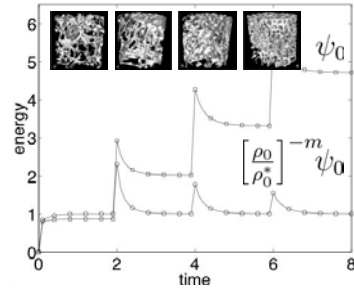
increasing forces causes density increase

constitutive equations

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density growth - mass source

$$D_t \rho_0 = \mathcal{R}_0 \quad f \leftarrow \text{bone diagram} \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$$



first time interval $f = 0.5N$

$$u = 1.5910l \quad \varphi = X + u = 2.5910l$$

$$F = \frac{\partial \varphi}{\partial X} = \frac{\partial 2.5910l}{\partial l} = 2.5910 \text{ homog.}$$

$$E = 1 \quad \lambda_0 = \frac{E\nu}{[1+\nu][1-2\nu]} = 0$$

$$\nu = 0 \quad \mu_0 = \frac{E}{2[1+\nu]} = 0.5$$

$$\psi_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^n \frac{1}{2} \mu_0 [F^2 - 1 - 2 \ln(F)]$$

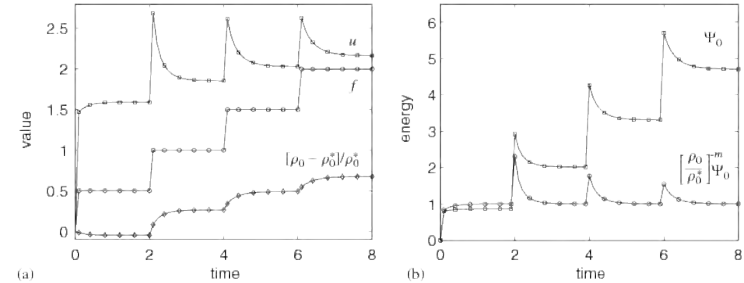
increasing force causes energy increase

constitutive equations

33

density growth - mass source

$$D_t \rho_0 = \mathcal{R}_0 \quad f \leftarrow \text{bone diagram} \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$$



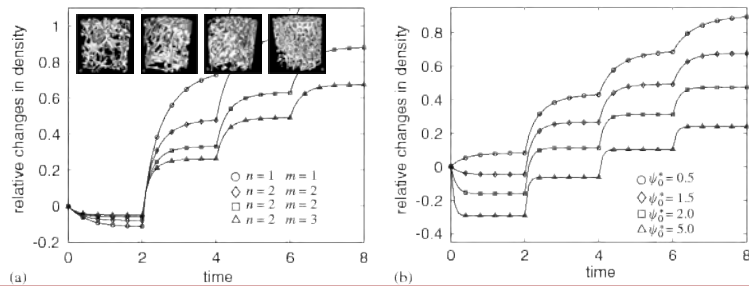
convergence towards biological equilibrium $D_t \rho_0 = 0$

constitutive equations

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density growth - mass source

$$D_t \rho_0 = \mathcal{R}_0 \quad f \leftarrow \text{bone diagram} \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$$



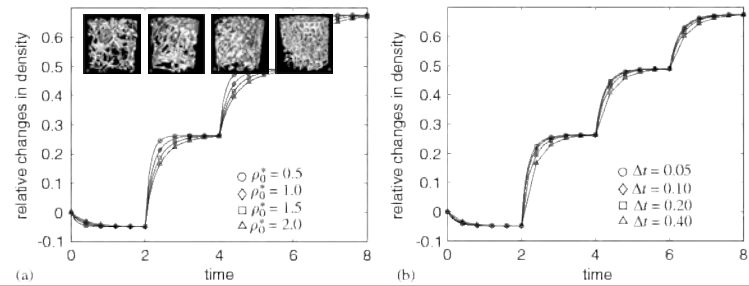
parameter sensitivity wrt n, m, ψ_0^*

constitutive equations

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density growth - mass source

$$D_t \rho_0 = \mathcal{R}_0 \quad f \leftarrow \text{bone diagram} \rightarrow f \quad \mathcal{R}_0 = \left[\frac{\rho_0}{\rho_0^*} \right]^{-m} \psi_0 - \psi_0^*$$

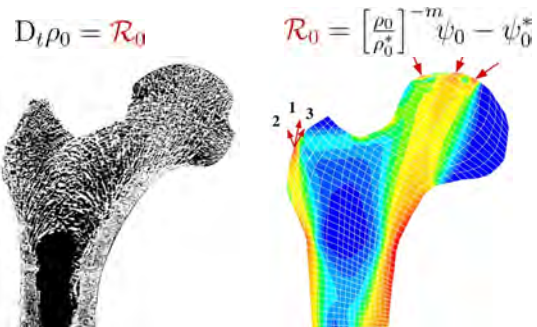


parameter insensitivity wrt $\rho_0^*, \Delta t$

constitutive equations

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density growth - mass source



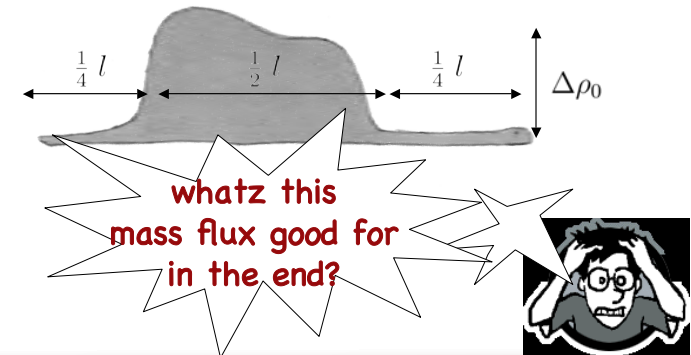
the density develops such that the tissue can just support the given mechanical load

constitutive equations

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density growth - mass flux

$D_t \rho_0 = \text{Div}(\mathbf{R})$ $\mathbf{R} = R_0 \nabla_X \rho_0$
initial hat type density distribution

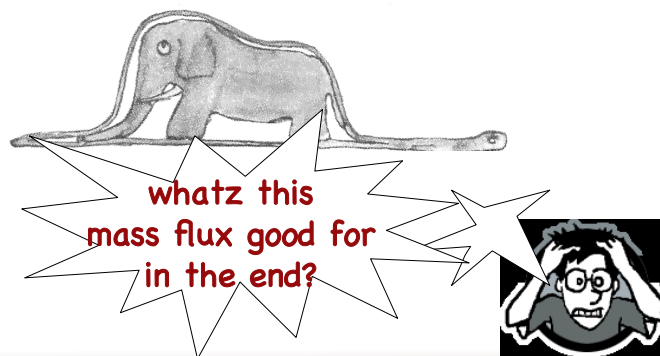


constitutive equations

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density growth - mass flux

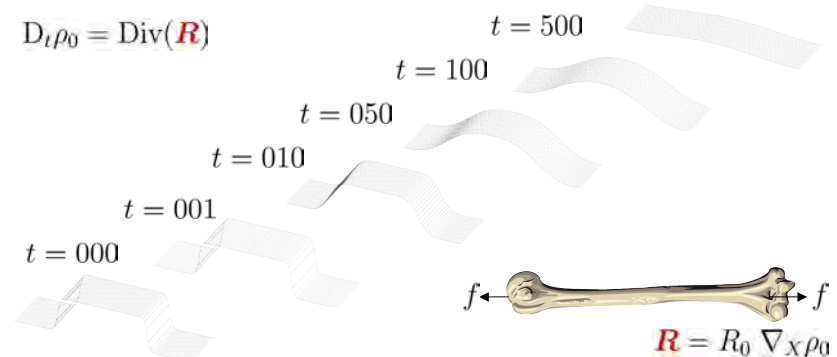
$D_t \rho_0 = \text{Div}(\mathbf{R})$ $\mathbf{R} = R_0 \nabla_X \rho_0$
initial hat type density distribution



constitutive equations

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density growth - mass flux

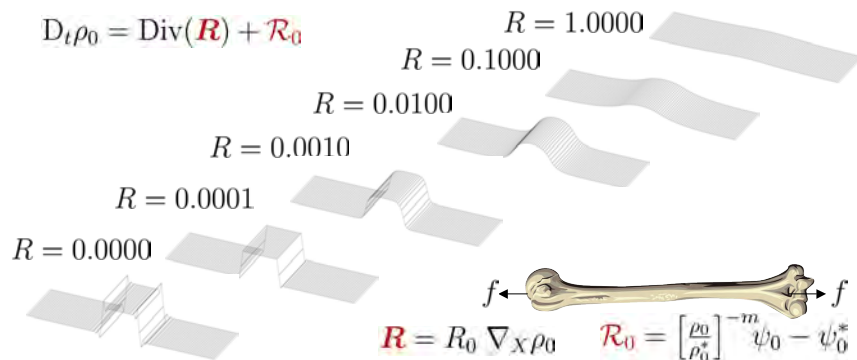


equilibration of concentrations

constitutive equations

40

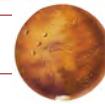
density growth - mass flux & source



smoothing influence of mass flux

constitutive equations

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density growth - bone loss in space



human spaceflight to mars could become a reality within the next 25 years, but not until some physiological problems are resolved, including an alarming loss of bone mass, fitness and muscle strength. gravity at mars' surface is about 38 percent of that on earth. with lower gravitational forces, bones decrease in mass and density. the rate at which we lose bone in space is 10-15 times greater than that of a post-menopausal woman and there is no evidence that bone loss ever slows in space. further, it is not clear that space travelers will regain that bone on returning to gravity. during a trip to mars, lasting between 13 and 30 months, unchecked bone loss could make an astronaut's skeleton the equivalent of a 100-year-old person.



<http://www.acsm.org>

example - bone loss in space

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density growth - bone loss in space



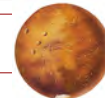
$$D_t \rho_0 = \mathcal{R}_0 \quad \mathcal{R}_0 = c \frac{\rho_0}{\psi_0^*} [\psi_0 - \psi_0^*]$$

nasa has collected data that humans in space lose bone mass at a rate of $c = 1.5\%/month$ so far, no astronauts have been in space for more than 14 months but the predicted rate of bone loss seems constant in time. this could be a severe problem if we want to send astronauts on a 3 year trip to mars and back. how long could an astronaut survive in a zero-g environment if we assume the critical bone density to be $\rho_0^{\text{crit}} = 1.00 \frac{\text{g}}{\text{cm}^3}$? you can assume an initial density of $\rho_0^* = 1.79 \frac{\text{g}}{\text{cm}^3}$!



example - bone loss in space

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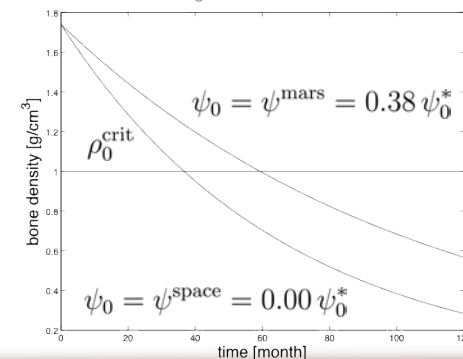


density growth - bone loss in space



$$D_t \rho_0 = c \rho_0 \left[\frac{\psi_0}{\psi_0^*} - 1 \right] \quad D_t \rho_0 = \frac{1}{\Delta t} [\rho_0^{n+1} - \rho_0^n]$$

$$\rho_0^{n+1} = \rho_0^n + c \rho_0^n \left[\frac{\psi_0}{\psi_0^*} - 1 \right] \Delta t \quad \rho_0(t_0) = 1.79 \frac{\text{g}}{\text{cm}^3}$$



$$\rho_0(36) = 1.0098$$

$$\rho_0(37) = 0.9947$$



example - bone loss in space

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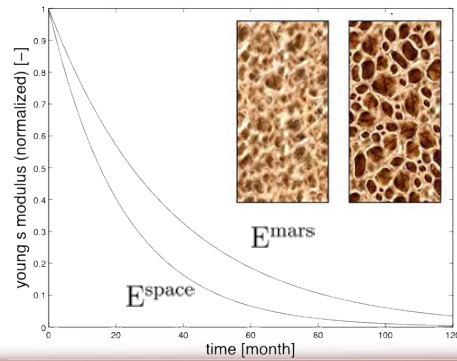


density growth - bone loss in space



$$E = 3.790 \rho_0^3 \text{ MPa} \quad \text{with } \rho_0 \text{ in g/cm}^3$$

carter & hayes [1977]



example - bone loss in space